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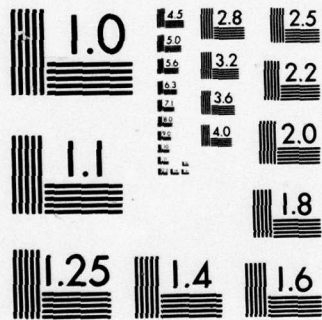
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NAVAL POSTGRADUATE SCHOOL
Monterey, California



THESIS

DEVELOPMENT OF A FLEXURAL DISK
TRANSDUCER FOR ACOUSTIC TRACKING
OF UNDERWATER VEHICLES

by

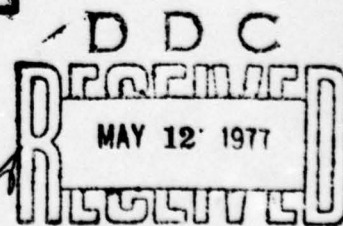
Omer SEVDIK

December 1976

Thesis Advisor:

O. B. Wilson

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DEVELOPMENT OF A FLEXURAL DISK TRANSDUCER FOR ACOUSTIC
TRACKING OF UNDERWATER VEHICLES

by

Omer SEVDIK
Lieutenant, Turkish Navy
B.Sc.E.A., Naval Postgraduate School, 1976

Submitted in partial fulfillment of the
requirements for the degree of

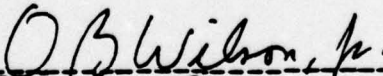
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December 1976

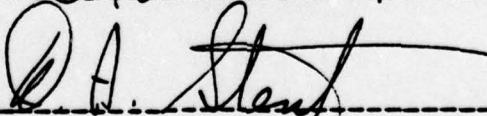
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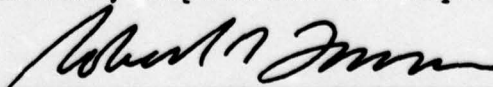
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Dean of Science and Engineering

ABSTRACT

A high frequency, broad-band transducer which has a broad radiation pattern in a half space is required for acoustic tracking of underwater vehicles. Two models of a flexural disk transducer, were built and tested. It was found that the radiation loading in water completely damps the resonances due to standing flexural waves and the radiation appears to be due entirely to flexural waves propagating in the disk. Broad-band radiation patterns and broad bandwidth (60-80 kHz) were obtained. The discrepancies between theory and experiment are attributed in part to violation of the thin plate assumptions and to lack of knowledge of the actual velocity distributions. This approach offers promise for achieving the desired broad beam widths. However, additional development work is needed to obtain a transducer which has the curved face necessary for smooth hydrodynamic flow.

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I. INTRODUCTION

For observing the position of submerged targets on underwater ranges, target-mounted sound sources are commonly used with fixed, bottom-mounted arrays. In order to insonify a large volume of water, essentially non-directional sources are required.

Considering the geometry of one tracking range, that at the Naval Torpedo Station (NTS), Keyport, Washington, which has a typical vertical distance of 200 m and the distance between bottom-mounted hydrophone arrays of about 2000 meters, the maximum slant range, r , can be found to be 1020 m. Using the following formula for transmission loss (TL), the transmission loss at the range, r , can be calculated:

$$TL = 20 \log r + a \cdot r$$

For a sound frequency of 75 kHz, the attenuation coefficient, a , for sea water is about 0.03 dB per meter. The transmission losses are 91 and 52 dB at ranges of 1020 and 200 m, respectively; hence, directional properties of the target-mounted sound source must compensate for this 40 dB difference in TL. Consideration of the pitch and roll motions of the underwater vehicle and the effect of the reflection from the surface has led to the specification that the source radiate uniformly within a conical volume 150 degrees wide, centered on the vertical axis of the transducer.

The practical shape of the beam pattern is shown in Fig 1 has been calculated considering the difference in transmission loss with angle.

In order to obtain the necessary source level at 75 degrees from the main axis, it is required to drive the transducer at large amplitudes. This however, apparently has shortened transducer life (From informal communication with NTS); accordingly redistribution of total energy away from main axis was a major design consideration. It is felt that this would extend the Mean Time Between Failure (MTBF) of the transducer and associated amplifiers.

Sufficient bandwidth for pulse code modulated telemetry and economy of the construction were additional goals.

Formerly, this requirement was met by a pop-out transducer, utilizing a spherical piezoelectric ceramic element. However, for current high-speed targets the performance of the protruding radiator is unsatisfactory, due principally to fluid flow problems. Therefore, a number of designs of flush mount transducers have been built and used for this purpose.

One approach to obtaining a broad beam radiation pattern is the use of a two element concentric piston transducer with amplitude and phase shading has been studied and which appears to offer promise (Ref. 4). Another approach is that of Mr. M. Barlow, at the Naval Torpedo Station, who proposed the idea of and carried out some initial experiments using flexural waves in a small disk for this purpose (private communication).

The intent of this study has been to explore further the use of transverse (flexural) vibrations in a plate as an approach in the development of a flush-mount transducer

capable of generating broad beam patterns at high frequencies.

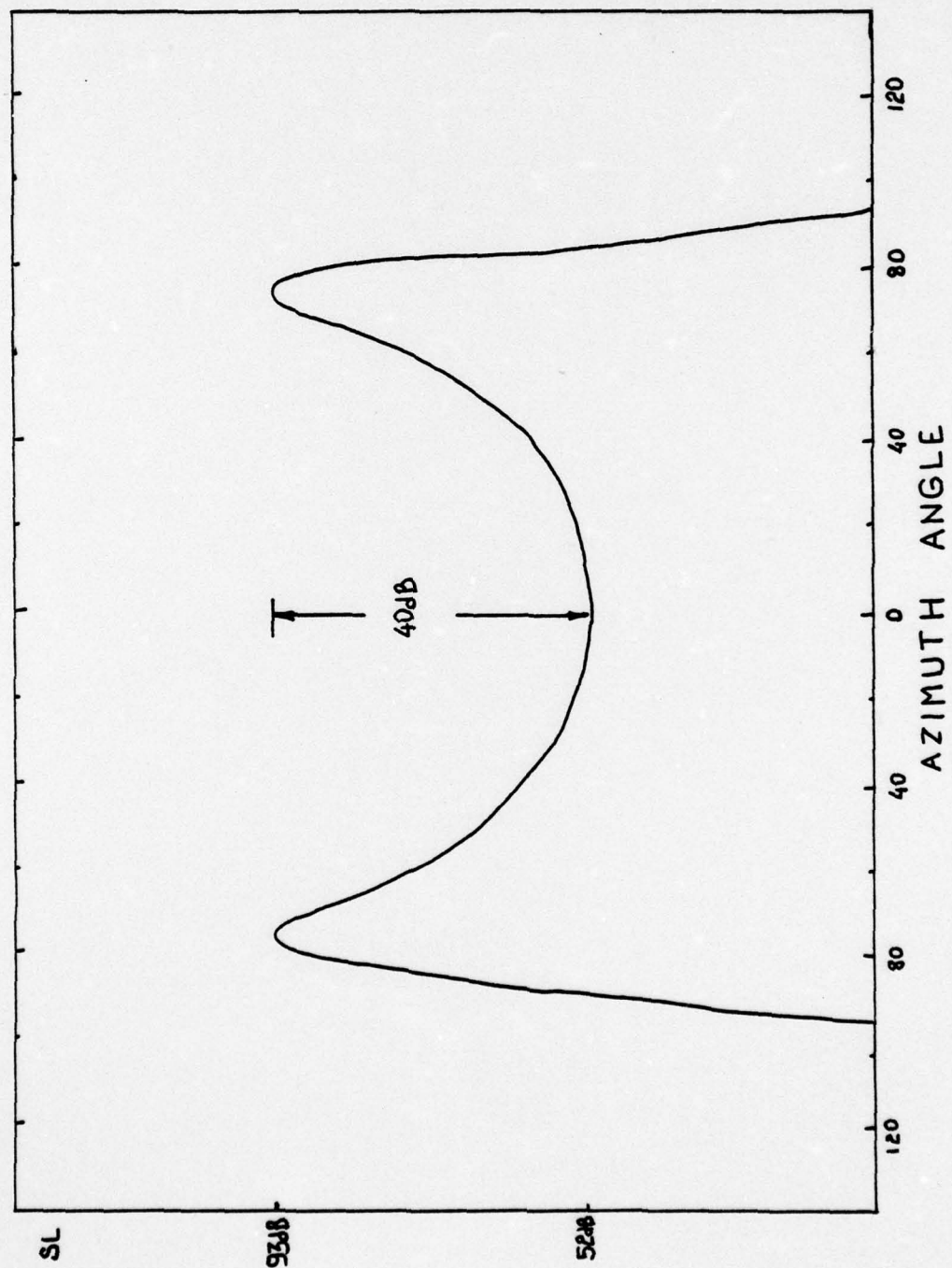


Figure 1 - PRACTICAL RADIATION PATTERN

II. THEORETICAL CONSIDERATIONS

The derivation of the transverse wave equation for thin plates is given in texts on theory of elasticity (Ref. 1 p. 214). The equation is,

$$\nabla^4 w + \frac{3\rho(1-s^2)}{Q h^2} \cdot \frac{\partial^2 w}{\partial t^2} = 0 \quad 2.1$$

where w is the displacement in the transverse direction, ρ is the density of the material, s is the Poisson's ratio, Q is the modulus of elasticity (Young's Modulus) and h is the half thickness of the plate. It has been assumed that h is small compared to the transverse wave length.

For simple harmonic motion of a plate,

$$w = Y(r, \phi) e^{-i2\pi f t}$$

and a differential equation for Y can be written:

$$(\nabla^2 - \gamma^2) (\nabla^2 + \gamma^2) Y = 0$$

where

$$\gamma = \frac{12\pi^2 f^2 \rho (1-s^2)}{Q h^2}$$

The solution of the first equation in polar coordinates, which is finite at $r = 0$, is,

$$Y = \frac{\cos(m\phi)}{\sin(m\phi)} J_m(\gamma r)$$

where m is an integer. The solution of the second equation is obtained from the first equation by changing γ into $i\gamma$. It is called the Hyperbolic Bessel Function and is defined as

$$I_m(z) = i^{-m} J_m(iz) .$$

Possible solutions for the simple harmonic oscillations of a plate are therefore given by the following expression:

$$Y(r, \phi) = \frac{\cos(m\phi)}{\sin(m\phi)} \left[A J_m(\gamma r) + B I_m(\gamma r) \right] .$$

A and B are derived from boundary conditions.

The boundary conditions for a circular plate of radius a , clamped its edges are:

$$Y(a, \phi) = 0 \quad \text{and} \quad \frac{\partial Y}{\partial r} = 0 \quad \text{at } r=a.$$

The first condition is satisfied by making

$$B = -A \frac{J_m(\gamma a)}{I_m(\gamma a)}$$

and the second condition is satisfied by requiring γ to satisfy

$$I_m(\gamma a) \frac{\partial}{\partial r} J_m(\gamma r) - J_m(\gamma a) \frac{\partial}{\partial r} I_m(\gamma r) = 0 \quad \text{at } r=a.$$

Because $\gamma = \gamma(f)$, this equation fixes the allowed frequencies.

One can label the solutions for this second condition:

$$\gamma_{mn} = \left(\frac{\pi}{a}\right) \beta_{mn}$$

where

$$\beta_{01}=1.015 \quad \beta_{02}=2.007 \quad \beta_{03}=3.000$$

A more complete tabulation of values of β_{mn} is given in Ref. 1, p. 215.

The allowed frequencies for the normal modes are;

$$f_{mn} = \frac{\pi h}{2a^2} \left[\frac{a}{3\rho(1-s^2)} \right]^{1/2} (\beta_{mn})^2 \quad 2.2$$

and the characteristic functions are:

$$\psi = \frac{\cos(m\phi)}{\sin(m\phi)} \left[\frac{J_m(\pi r \beta_{mn})}{I_m(\pi r \beta_{mn})} - \frac{J_m(\pi \beta_{mn})}{I_m(\pi \beta_{mn})} \frac{I_m(\pi r \beta_{mn})}{I_m(\pi \beta_{mn})} \right]$$

On the other hand, the transverse wave speed c_b for plate without losses is given at Ref 2, p. 508,

$$c_b = \omega^{1/2} \left(\frac{B}{M} \right)^{1/4}$$

where $B = \frac{Q (2h)^3}{12 (1-s^2)}$

is the stiffness of the plate for bending and M is the mass of the plate per unit surface.

The following expression gives the value of the plate half thickness:

$$h = \frac{c_b^2}{2\pi f \left[\frac{Q}{3\rho(1-s^2)} \right]^{1/2}} \quad 2.3$$

Hence, for a given frequency and plate material one can find a direct relationship between the thickness of the plate and the transverse wave speed c_b from equation 2.3. One can also find a relationship between the radius a and thickness $2h$ by using equation 2.2. In combining these two results the relationship between radius and thickness can be obtained.

For aluminum plates (Ref 3)

$$\rho = 2700 \text{ kg/m}^3$$

$$Q = 7.1 \cdot 10^{10} \text{ nt / m}^2$$

$$s = .33$$

For the (0,2) mode, and a frequency of 75 KHz

$$a^2 = 0.2627 \text{ h}$$

$$c_b^e = 1.47 \cdot 10^9 \text{ h}$$

Computation of the radiation pattern function was based on a variation of a program worked out by Shaw (Ref 4). In this case, the radiation pattern is the sum of radiations from a set of 20 concentric ring piston elements. An assumption is made about the amplitude and phase of the velocity of motion as a function of piston radius.

The pattern for any ring, say number n , which has outer and inner radii of a_n and a_{n-1} , respectively and a velocity amplitude U_n , is computed by subtracting the ordinary, uniform piston radiation pattern function of radius a_{n-1} with velocity amplitude U_n from that of a piston of radius a_n and velocity U_n .

A computer program shown in Appendix A was used to estimate the radiation patterns for combinations of various modes and radii.

None of the patterns so obtained were found to resemble the specifications described before in the introduction section, but only (0,2) mode offered some promise. One of the calculated radiation pattern is shown in Fig 2.

Also, radiation from circular progressive wave was estimated using the computer program given in Appendix B.

The equation for the displacement of an outgoing circular progressive flexural wave is:

$$w = A H_0^{(2)}(k_b r)$$

where $H_0^{(2)}$ = Hankel function of the second kind

Using the same method described above radiation patterns of various thickness and radius combinations were obtained. One of them is shown in Fig 3.

III. EXPERIMENTAL PROCEDURES

Based on the theoretical beam patterns, a plate with half thickness, $h=1.5$ mm and a radius $r=2.38$ cm, was chosen for a first try and the transducer shown in Fig 4 was constructed. Some dimensions were specified by the positioning and mounting hole for the transducer on the extender section of the test vehicle.

To drive this transducer, a hollow piezo-ceramic cylinder, with radial polarization which has following specifications was used :

Ceramic: GLENNITE HS21

Length: 1.0 in

Outer diameter: 0.5 in

Wall thickness : 0.125 in

Longitudinal resonance: 89.63 kHz

Using a composite transducer configuration with mass-loading on the ends due to two pieces of aluminum (Fig 5), the longitudinal resonance was reduced to 73.6 kHz. In order to attach the masses to the element a nut and bolt were used; however, for driving the plate the nut was found to be unnecessary. Without it, it was assumed that the longitudinal resonance would approach 75 kHz.

Upon completion of the construction, electrical

admittance measurements of the transducer were made using a Dranetz Impedance-Admittance meter. The result for the unloaded transducer (in air) is shown in Fig 6. Primary resonances were found at frequencies:

66.34 kHz, 73.26 kHz, 80.4 kHz, 105.2 kHz.

The configuration shown in (Fig 7) and a Capacitive Displacement Probe (Ref 4 Fig 35) which averages displacement over the probe face were used to determine the modes of vibration for each resonance. After careful (and difficult) measurements the amplitude distribution of 66.34 kHz was found to resemble closely that expected for the (0,2) mode. The distribution at 73.26 kHz resembled somewhat that expected for the (0,3) mode. However the pattern was not symmetrical. It is believed that this is one of the mixed-modes. Relative amplitude distributions are shown in Figs 8-10.

Next the transducer was placed in the extender section. In this instance, admittance measurements showed small deviations from earlier resonance frequencies; however, when the mounted transducer was placed into water, none of the earlier resonances were found, except for the one at 72.27 kHz. Both admittance curves appear in Fig 11. It appears that the radiation loading completely damps the normal modes of flexural vibration of the plate and that the resonance at 72.27 kHz is associated with the longitudinal vibration of the ceramic driver element.

Measurements of the radiation pattern of the transducer were made in one of the Naval Postgraduate School's anechoic water tanks using apparatus described below. The transducer was mounted in the wall of an aluminum cylinder which was the extender section of a 12-3/4 inches diameter torpedo.

The transducer baffle assembly can be rotated about a vertical axis. A potentiometer mounted on a shaft in the drive train provides an electrical signal which is proportional to angle of rotation which can be used to drive one axis of a graphical plotter.

In order to eliminate the effects of surface reflections, and minimize the effects of standing waves in the tank the pulse mode of operation was used. In this mode, the Boxcar Integrator, gated to the direct path pulse, generates a d.c voltage proportional to the amplitude of the pulse. This voltage is fed to a calibrated logarithmic converter which then generates the ordinate of the beam pattern in decibels. To improve signal to noise ratio (SNR), a high driving voltage (30 vrms or more) was used. The transducer and hydrophone were located with a two meter separation. The following test equipment was connected as shown in Fig 12:

Hewlett Packard 7035 B X-y Recorder

Tektronix RM45A Dual Trace Oscilloscope

Hewlett Packard 465A Voltage Amplifier

PAR 160 Boxcar Integrator

Krohn-Hite DCA 50R Power Amplifier

Harrison 6205 B D.C. Power Supply

40 dB. Gate

General Radio 1396A Tone Burst Generator

General Radio 1192B Frequency Counter

Hewlett Packard 204C Oscillator

Hewlett Packard 407A Power Amplifier

LC-10 Hydrophone

Envelope Detector

Hewlett Packard 7561A Logarithmic Converter

The radiation pattern for various frequencies are presented in Figs 13-21.

It is believed that the measured radiation patterns are due principally to the progressive transverse wave in the plate and not, as first theorized, to the existence of standing flexural waves in the plate.

The results show that radiation patterns below 60 kHz do approach the pattern which is shown earlier in Fig 1. However above 60 kHz, the level along the axis increases relative to that at larger angles. The broad beam width characteristics appear to change little with frequency.

A second transducer was built with a thicker plate (4 mm) which should result in a larger transverse wave speed.

Driving this new model (MOD 2) with the same ceramic element, the admittance curves shown in Figs 21-23 were obtained. The results were almost the same as earlier model. In water, the resonance was found at 72.24 kHz.

Using the same configuration of test instruments shown in Fig 12, reasonably good radiation patterns were obtained below 78 kHz for this new model (Figs 24-29).

In an attempt to understand better the details of motion of the vibrating plate when in water, near field pressure measurements were made using the following equipment:

Hewlett Packard 204C Oscillator

General Radio Frequency Counter

Hewlett Packard 467A Power Amplifier

Krohn Hite DCA 50R Power Amplifier

Tektronix RM45A Oscilloscope

LC-5 Hydrophone

Dranetz Phasemeter 305

Hewlett Packard 403B Voltmeter

The LC-5 hydrophone was placed about 1 or 2 mm from the face of the transducer in the anechoic tank. A rack and pinion assembly supporting the hydrophone permitted moving the hydrophone across the face of the transducer for near field measurements. Continuous excitation was used. The figures obtained for near field pressure amplitudes and phases are presented in Fig 30 and 31 for the MOD 1 transducer, and in Figs 32 and 33 for the MOD 2 transducer when driven at the resonance frequency. Another measurement made at 60 kHz driving frequency gave the results shown in Figs 34-35.

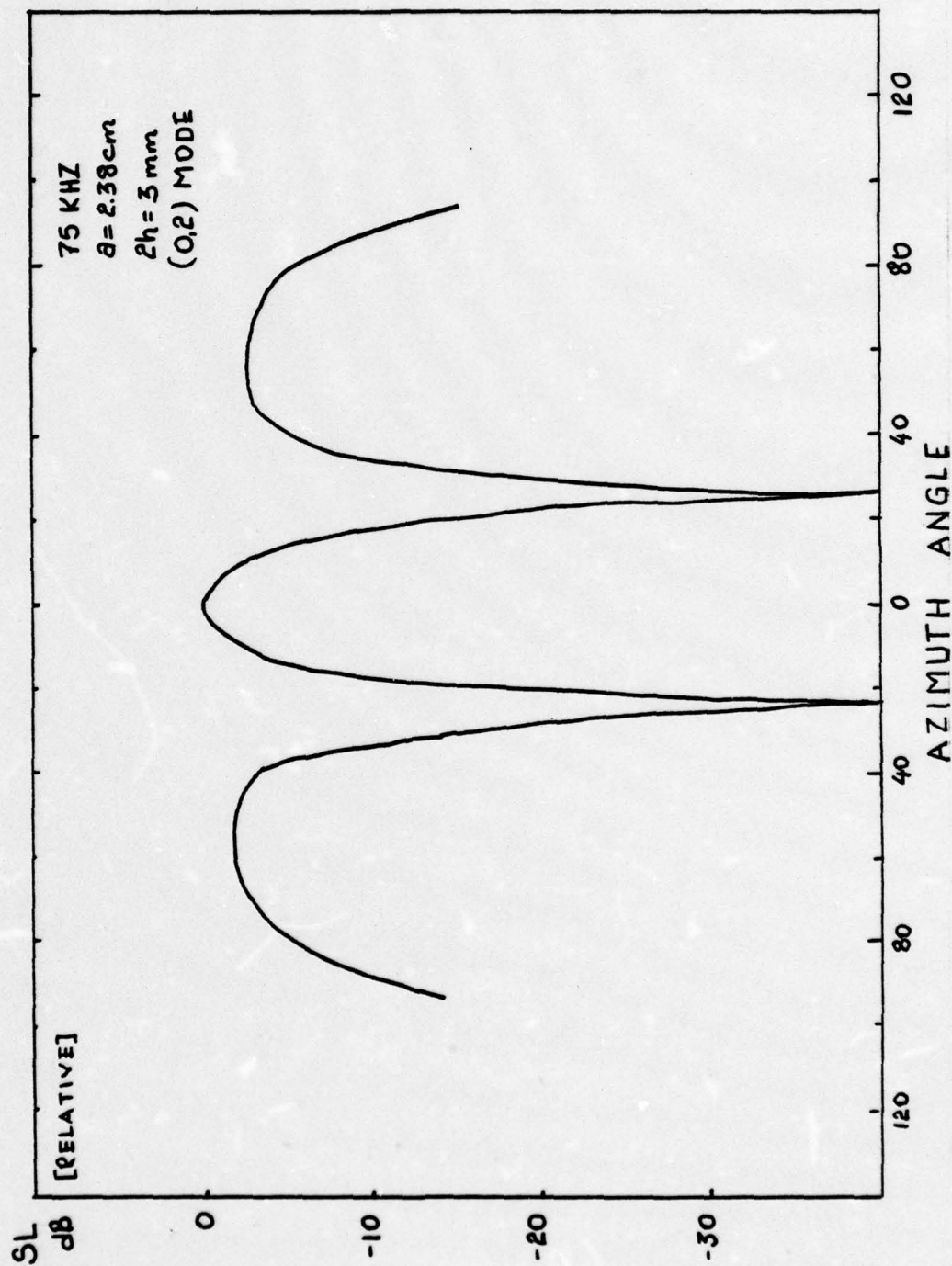


Figure 2 - CALCULATED RADIATION PATTERN USING NORMAL MODE SOLUTION

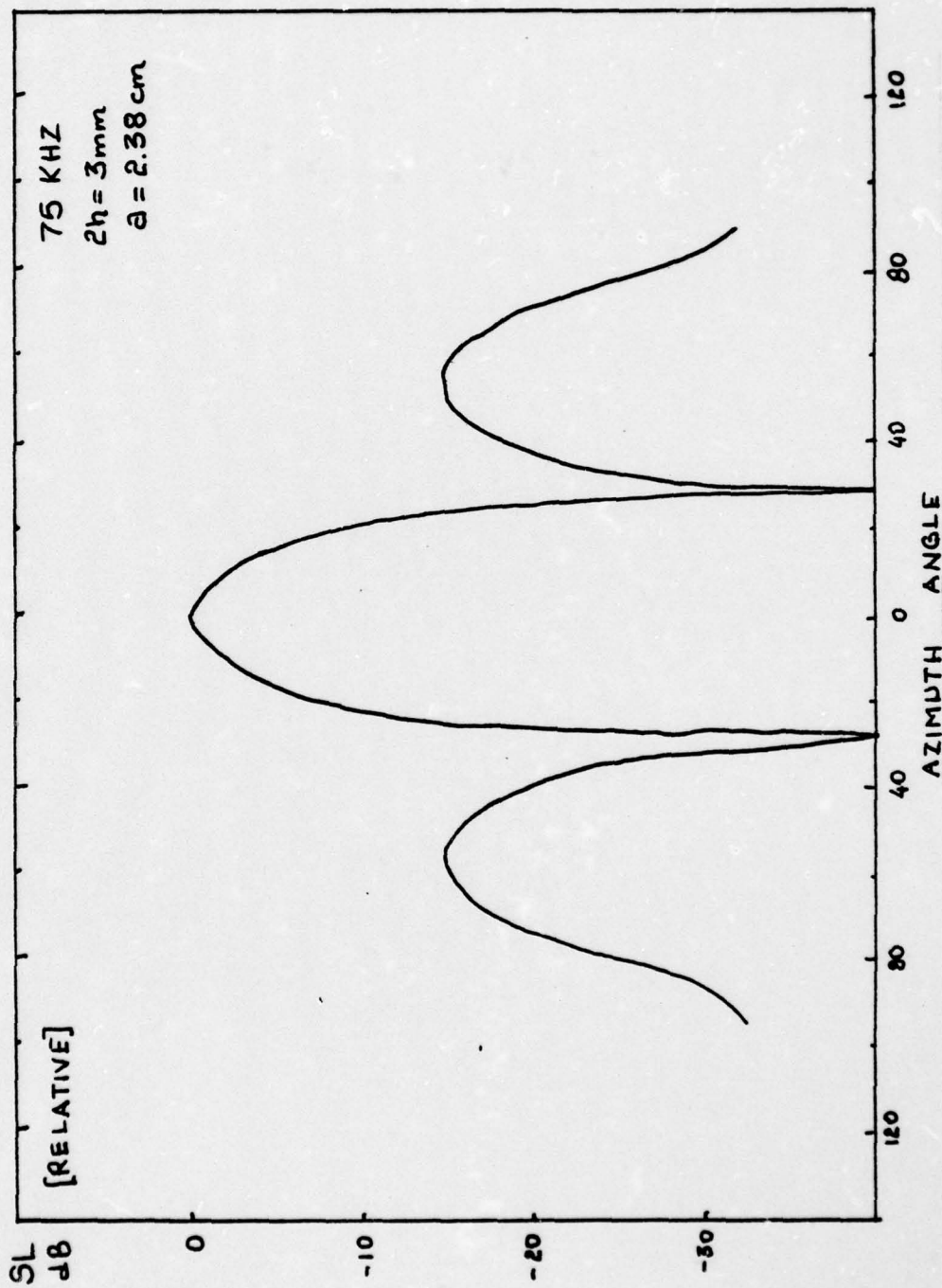


Figure 3 - CALCULATED RADIATION PATTERN USING PROGRESSIVE
 WAVE SOLUTION

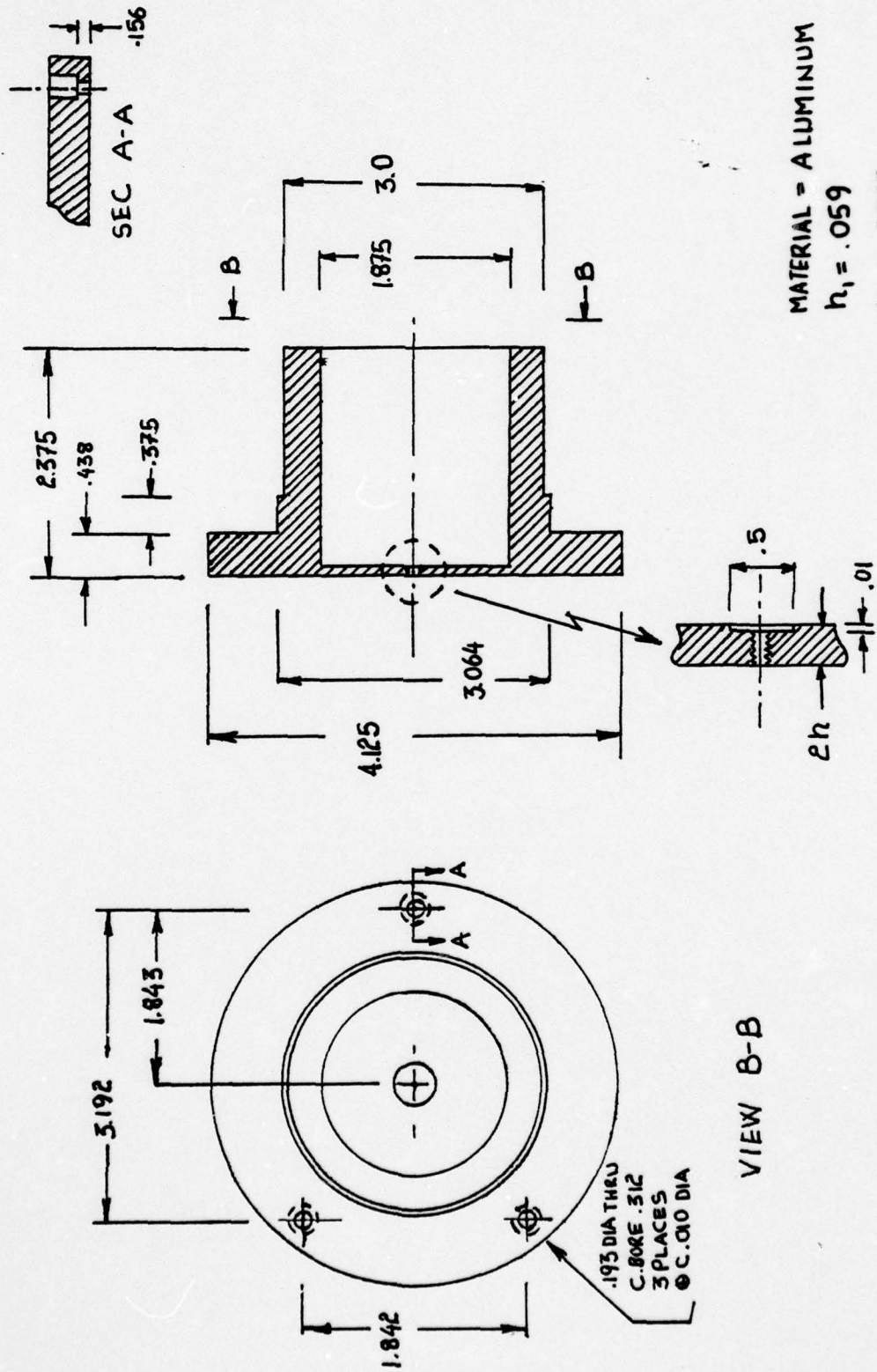
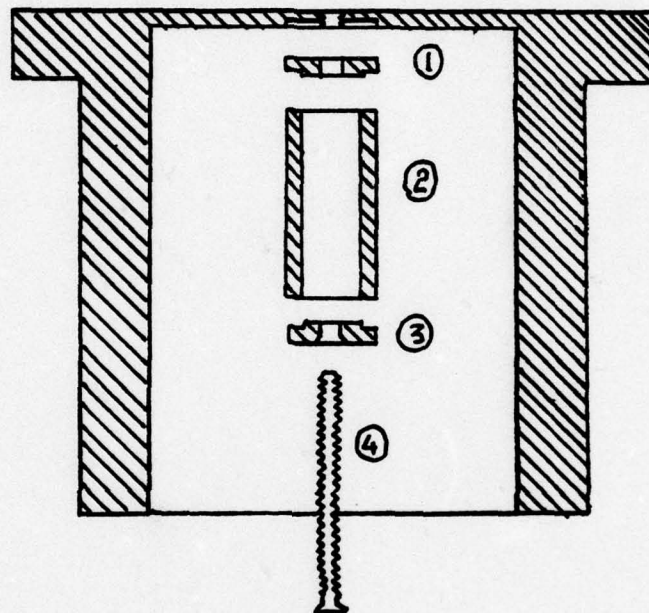


Figure 4 - TRANSDUCER DIMENSIONS



- ① AND ③ : ALUMINUM MASSES
② : CERAMIC ELEMENT
④ : SCREW

Figure 5 - TRANSDUCER AND DRIVING ELEMENT

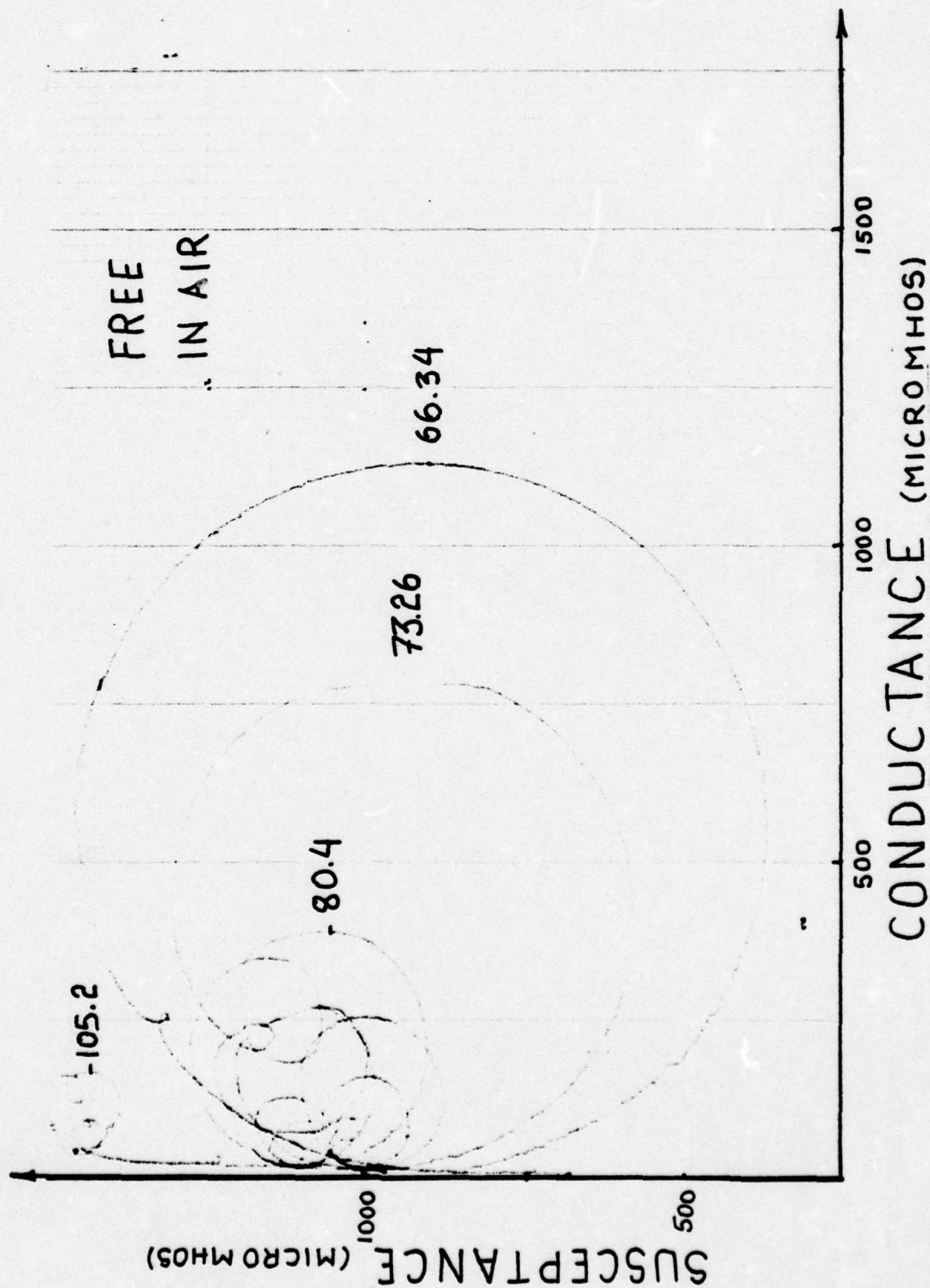


Figure 6 - ADMITTANCE IN AIR

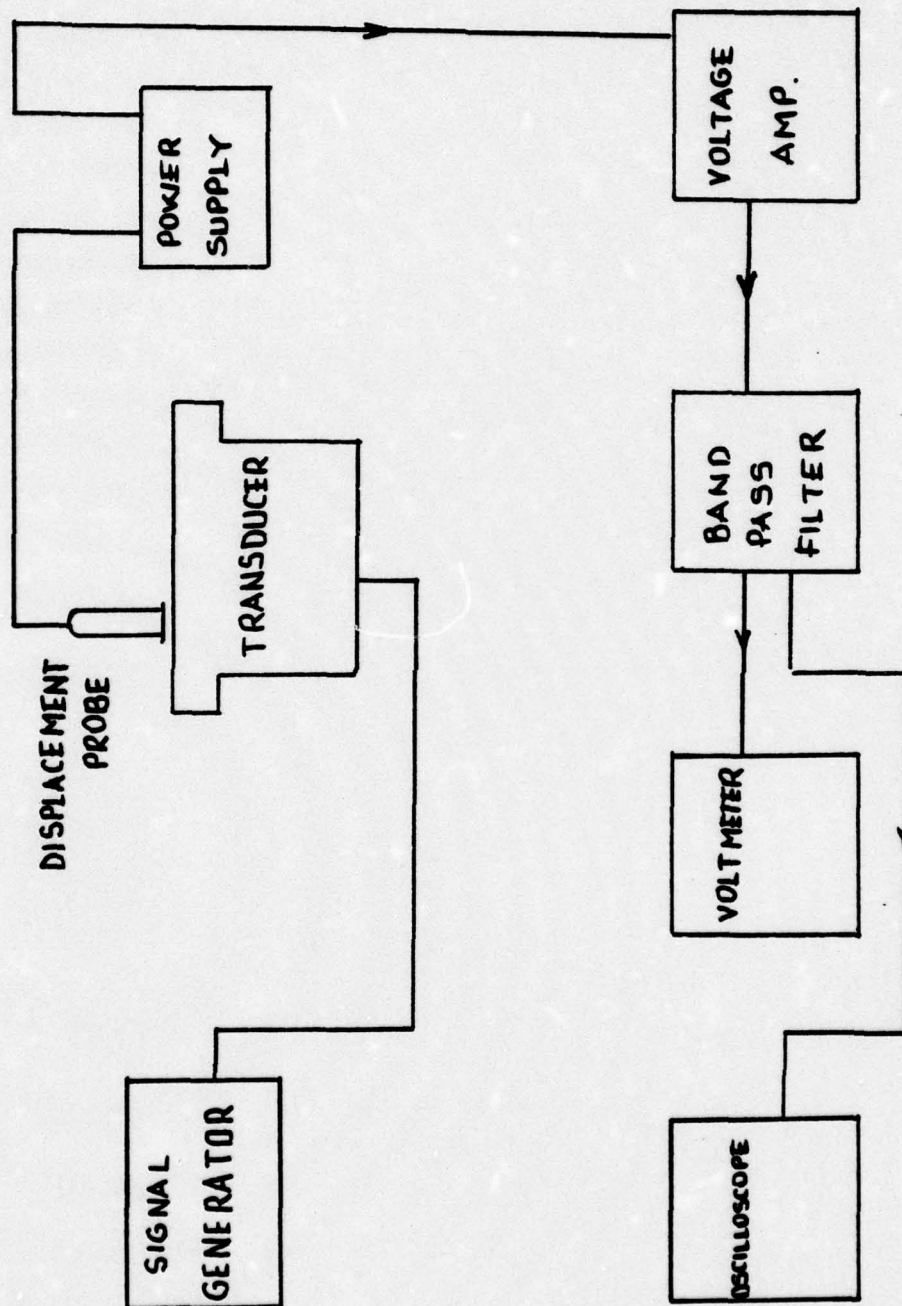


Figure 7 - DISPLACEMENT MEASUREMENTS

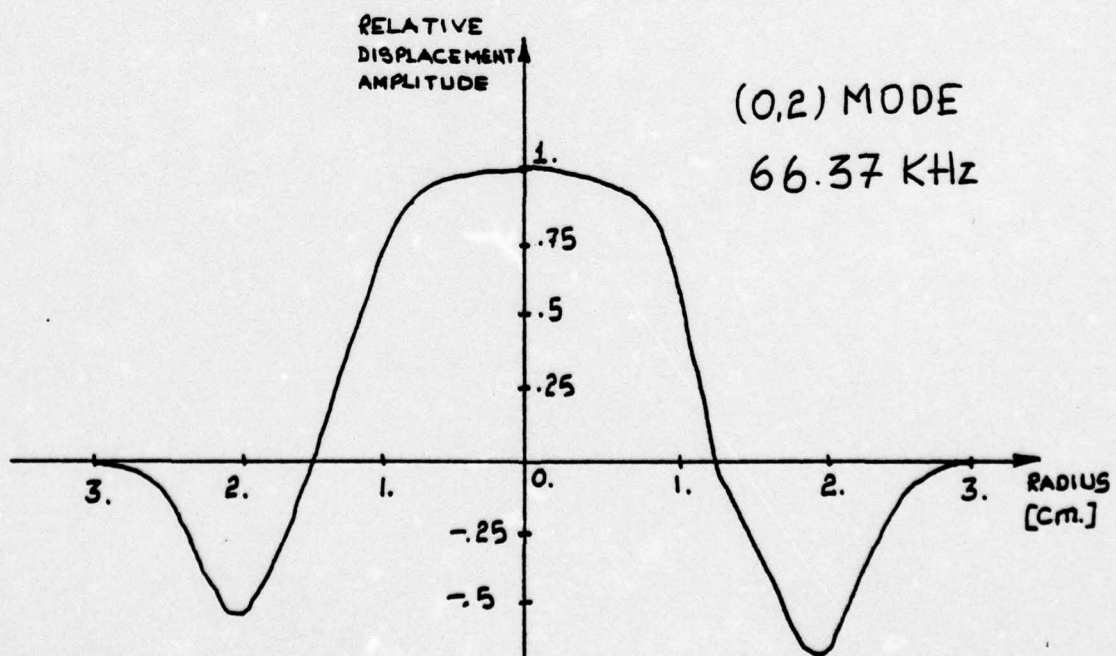
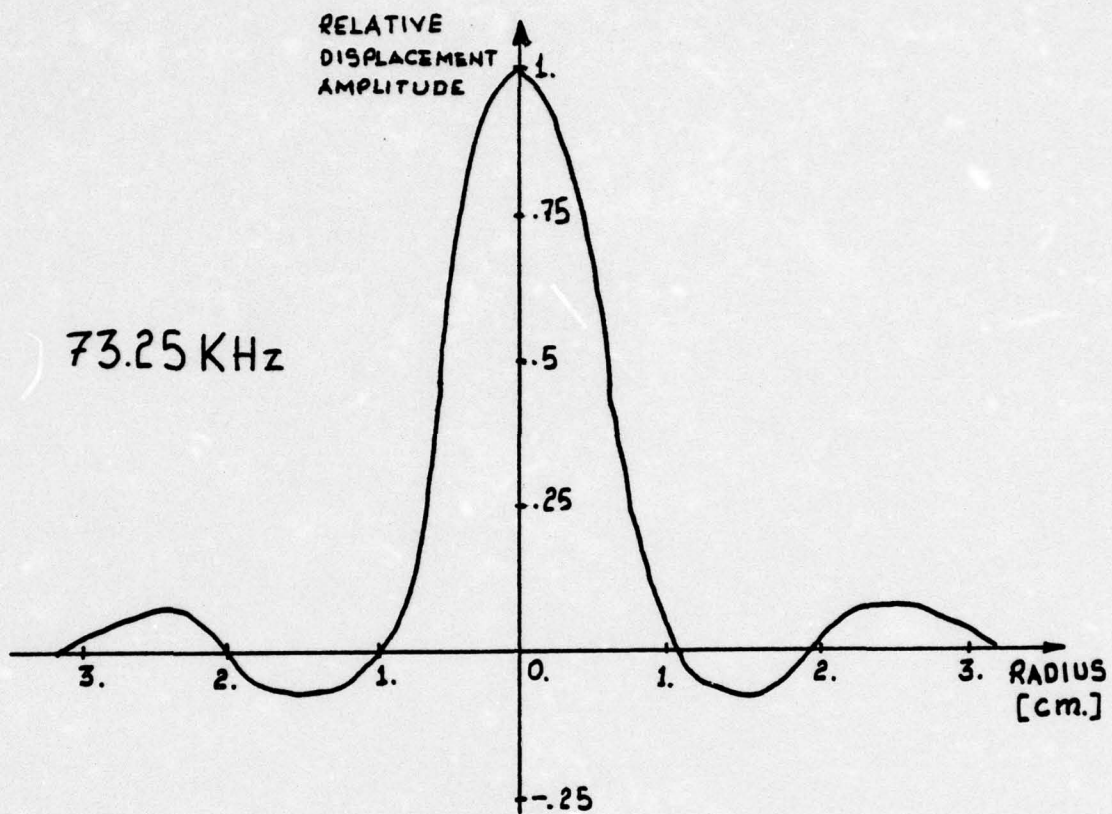


Figure 8 - RELATIVE DISPLACEMENT AMPLITUDES

(0.2) MODE AMPLITUDE DISTRIBUTION
66.37 KHz.

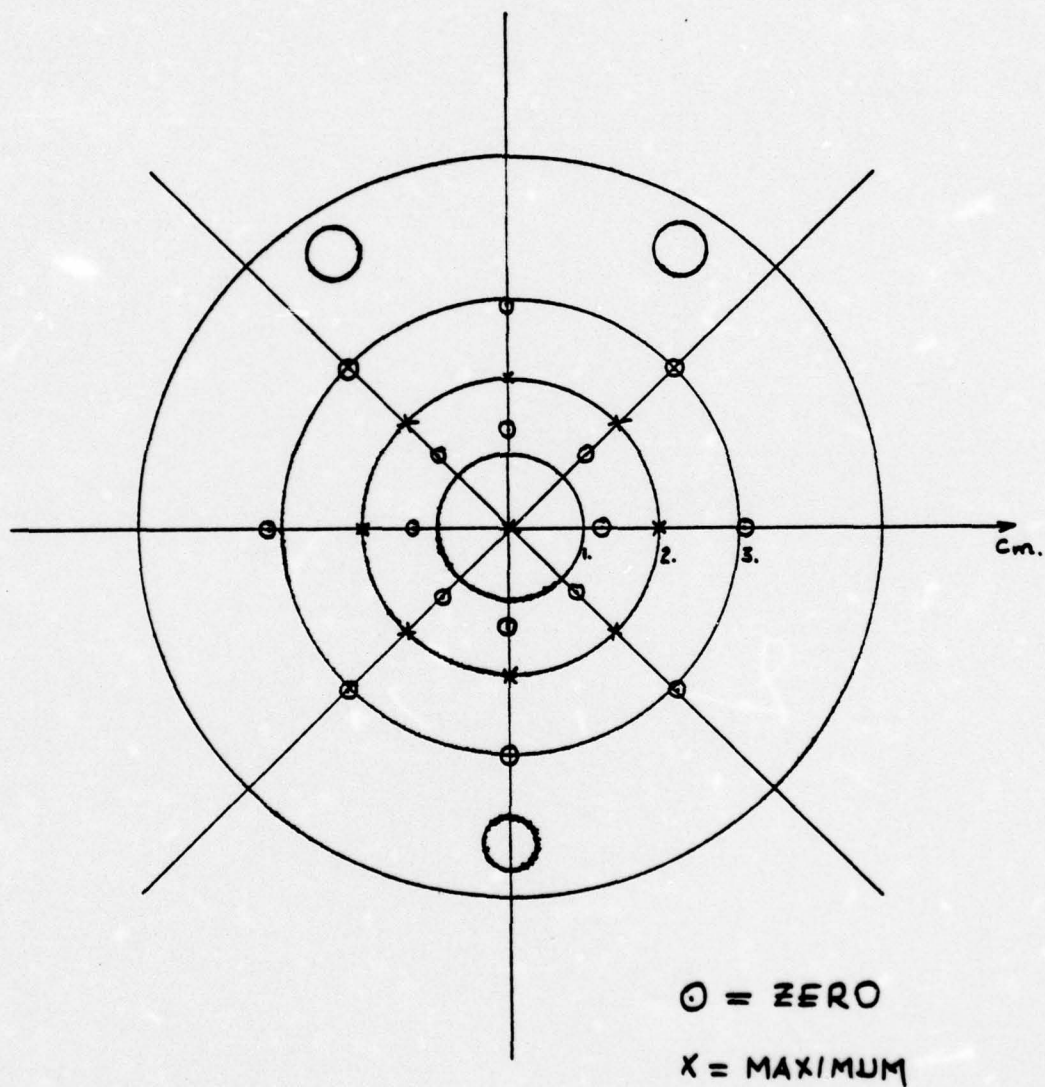


Figure 9 - AMPLITUDE DISTRIBUTION ON THE FACE OF THE
TRANSDUCER

AMPLITUDE DISTRIBUTION

73.24 KHz.

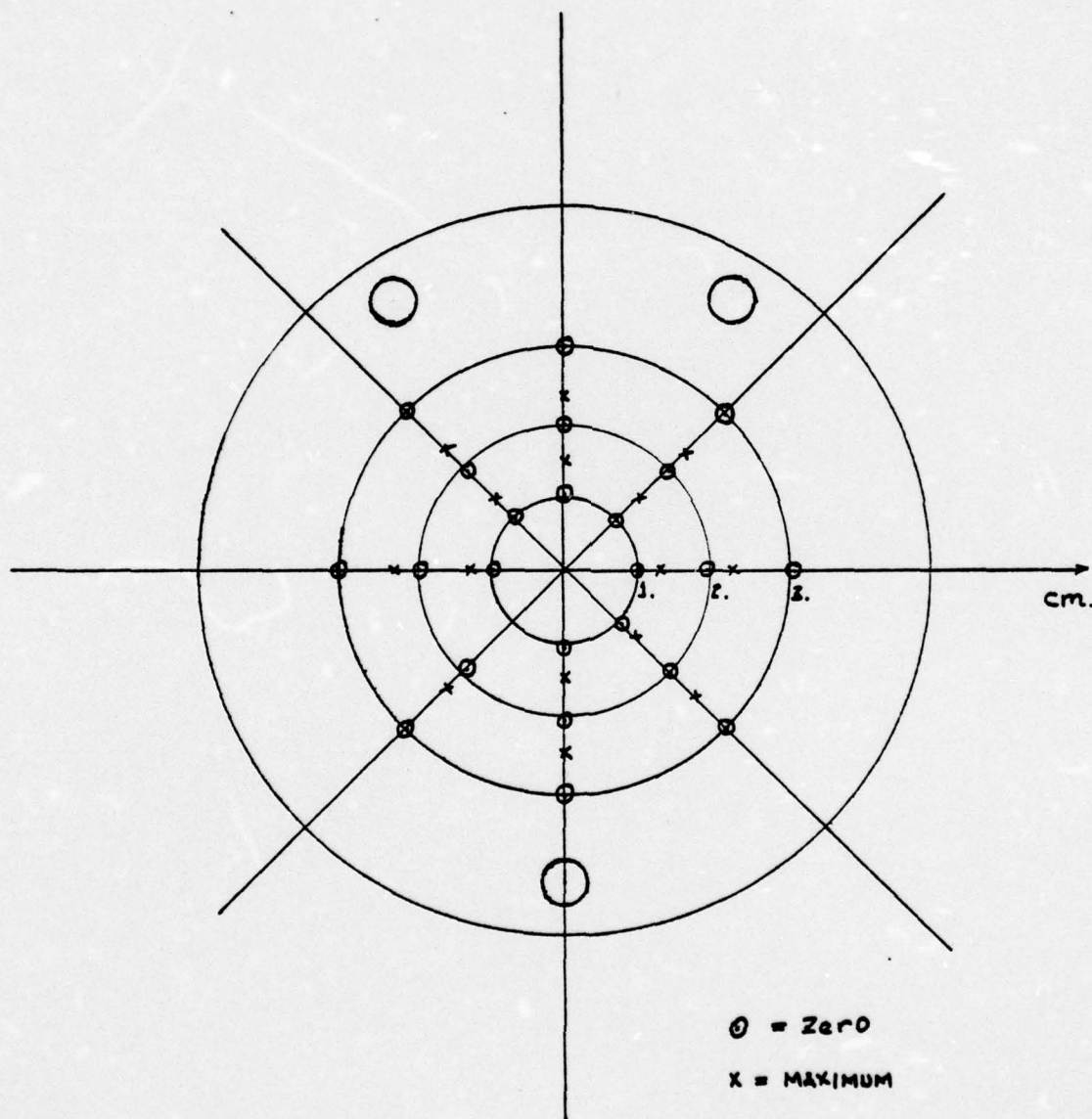
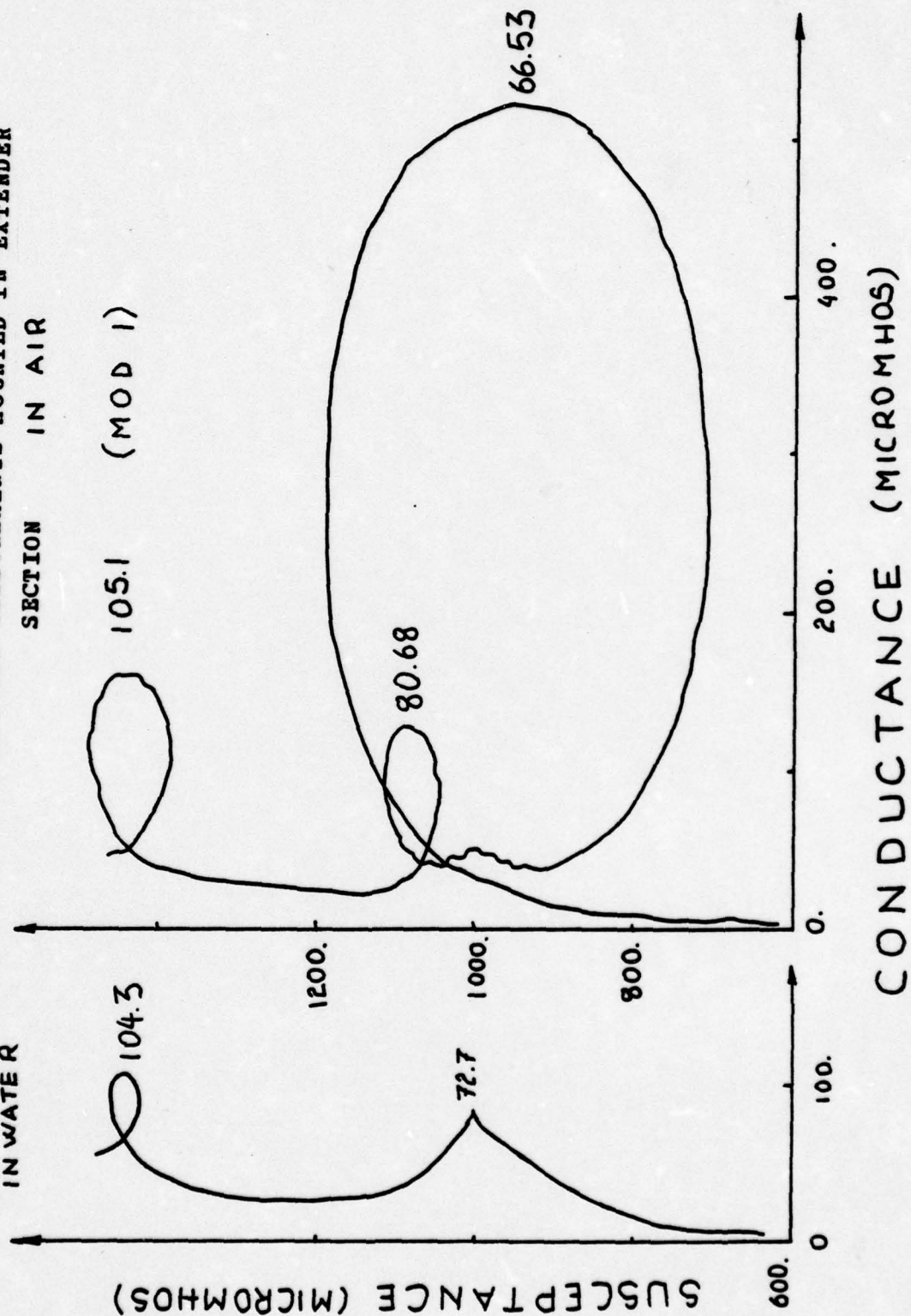


Figure 10 - AMPLITUDE DISTRIBUTION ON THE FACE OF THE
TRANSDUCER

Figure 11 - ADMITTANCE MEASUREMENTS MOUNTED IN EXTENDER
SECTION IN AIR



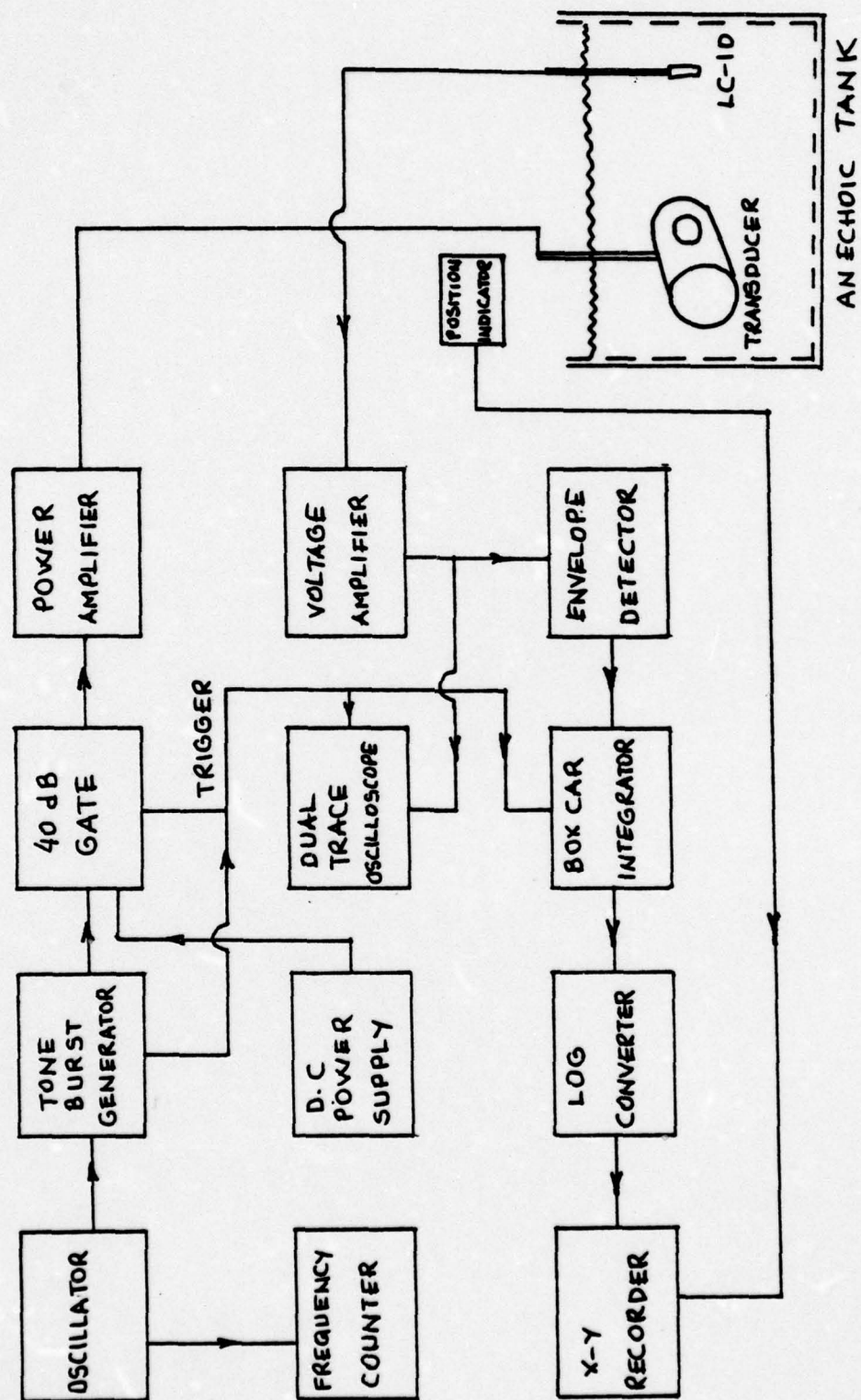


Figure 12 - APPARATUS FOR BEAM PATTERN MEASUREMENTS

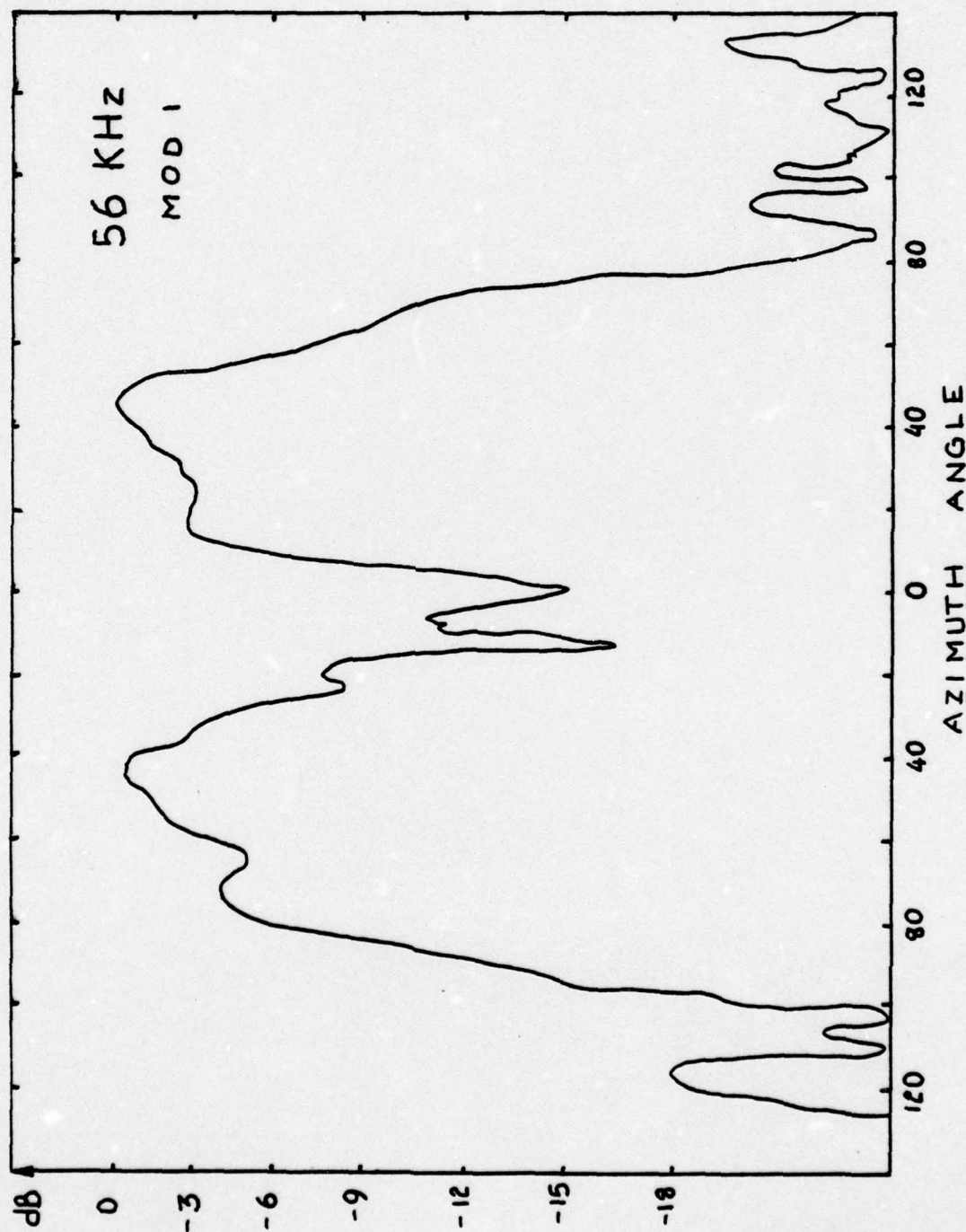


Figure 13 - RADIATION PATTERN

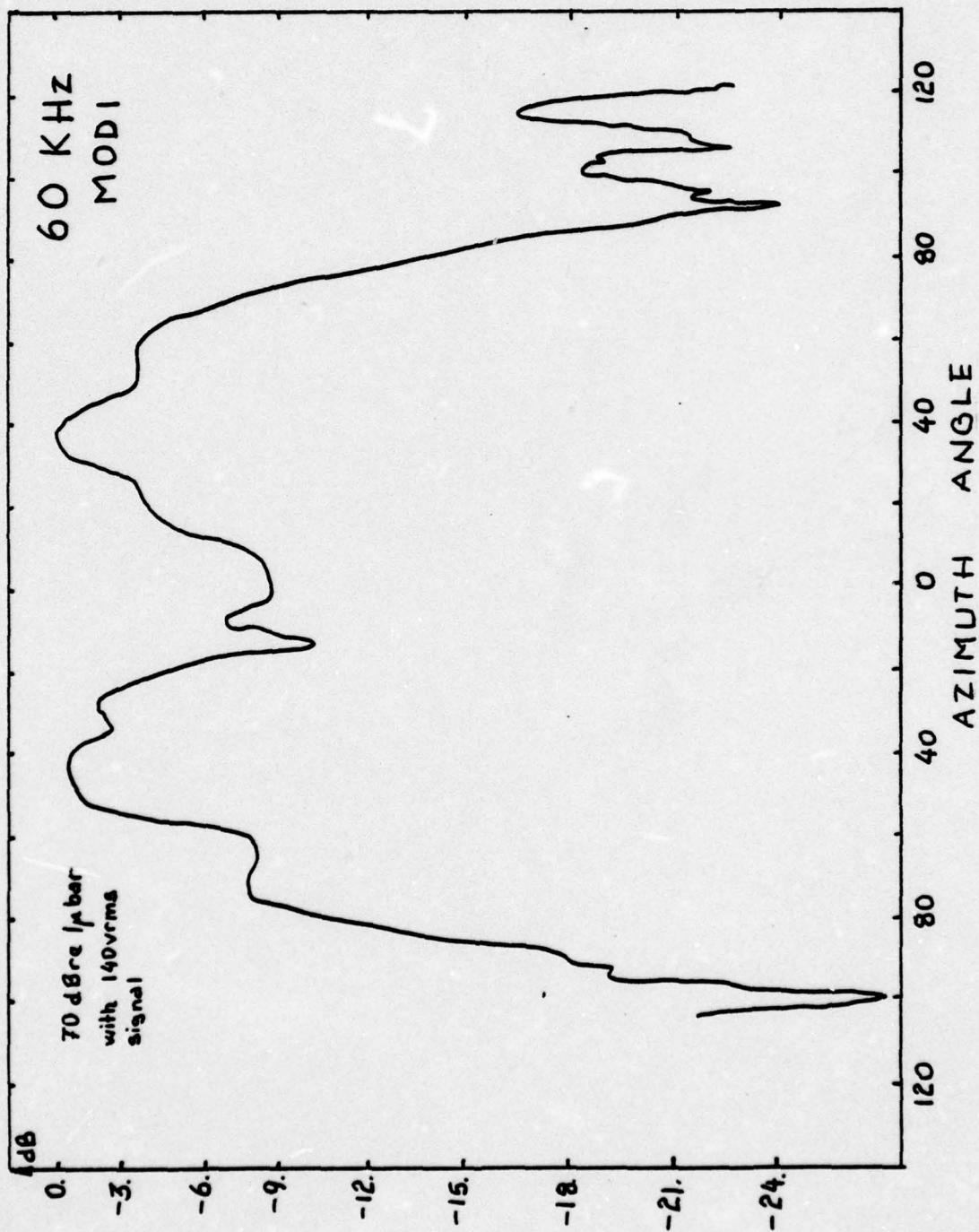


Figure 14 - RADIATION PATTERN

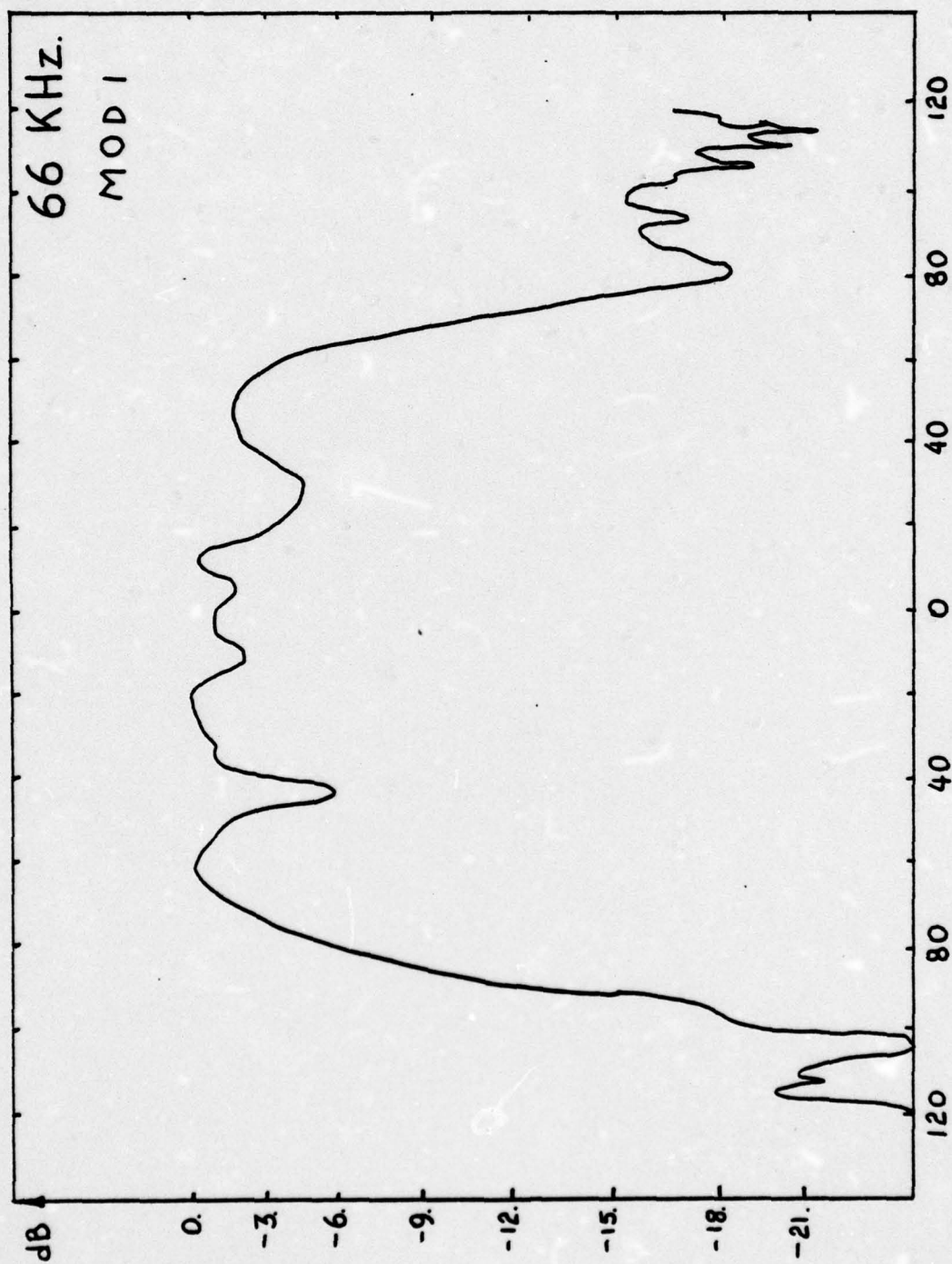


Figure 15 - RADIATION PATTERN

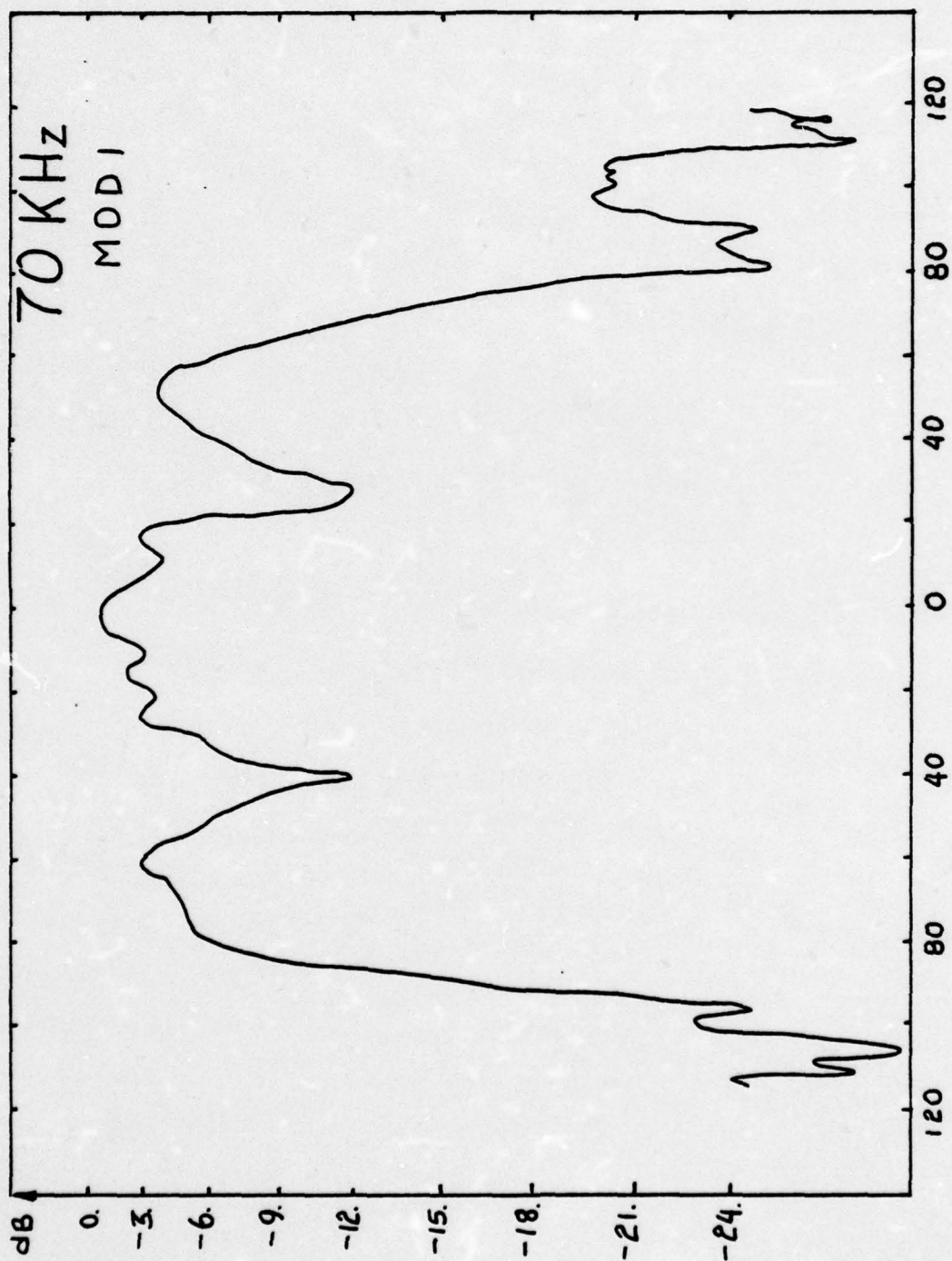


Figure 16 - RADIATION PATTERN

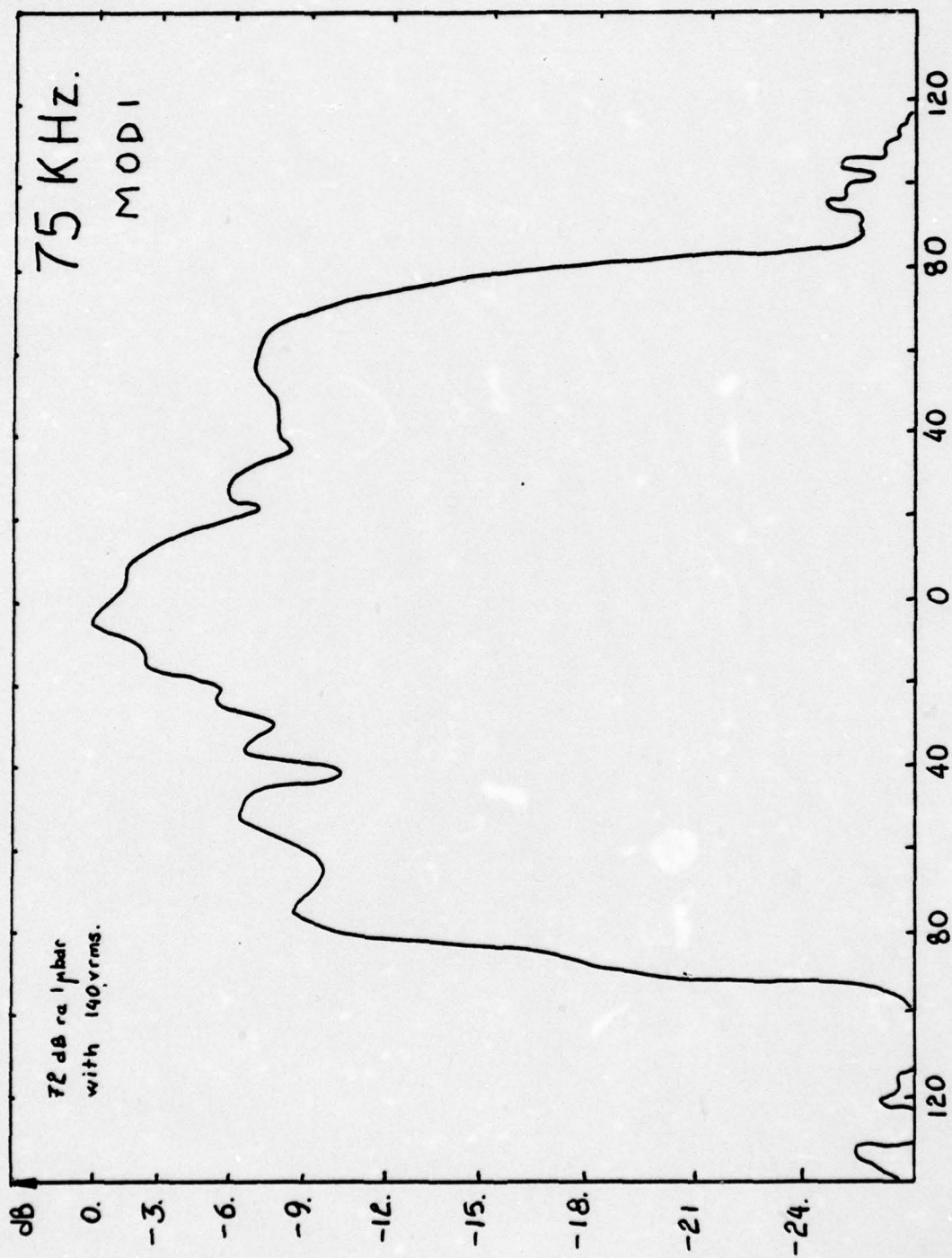


Figure 17 - RADIATION PATTERN

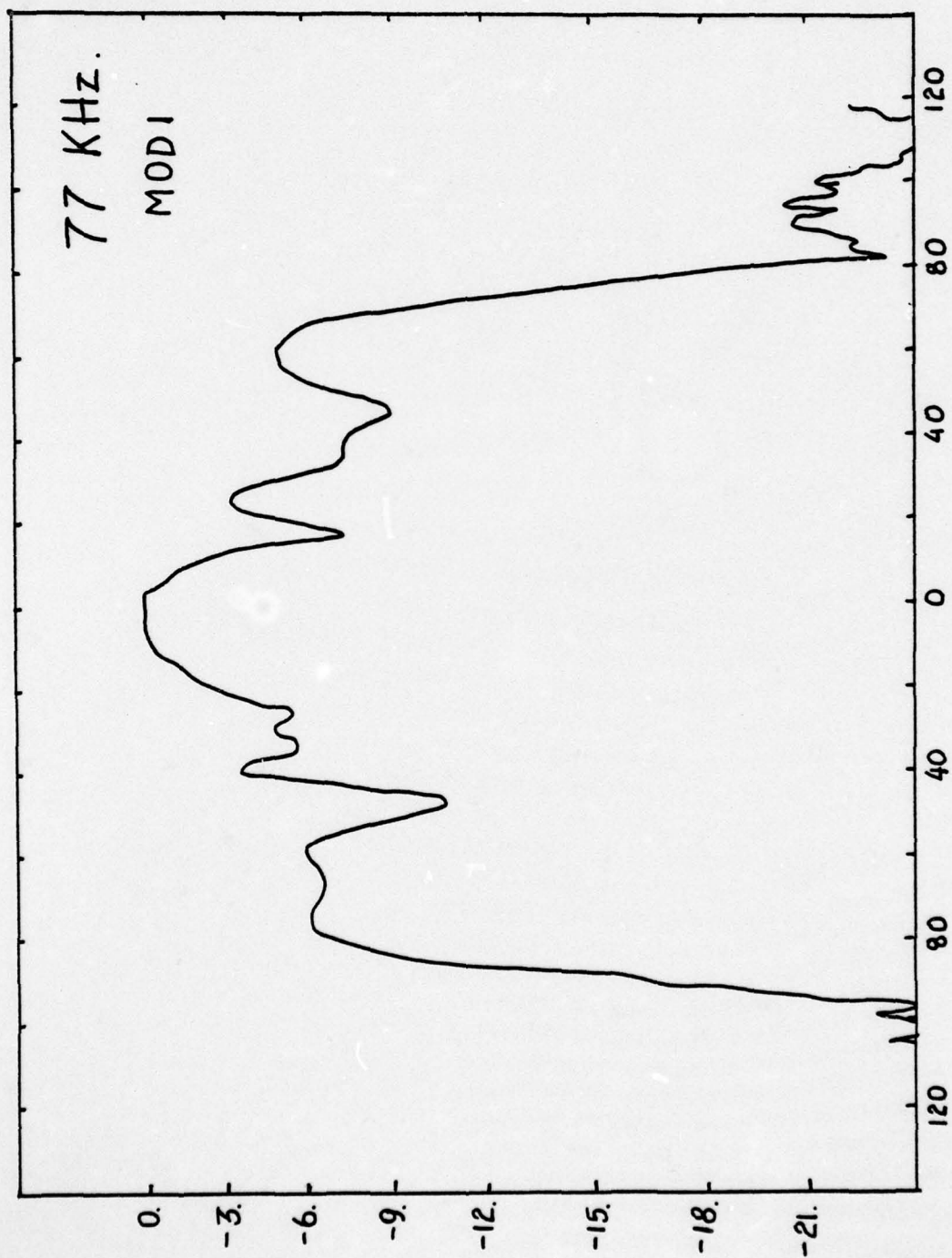


Figure 18 - RADIATION PATTERN

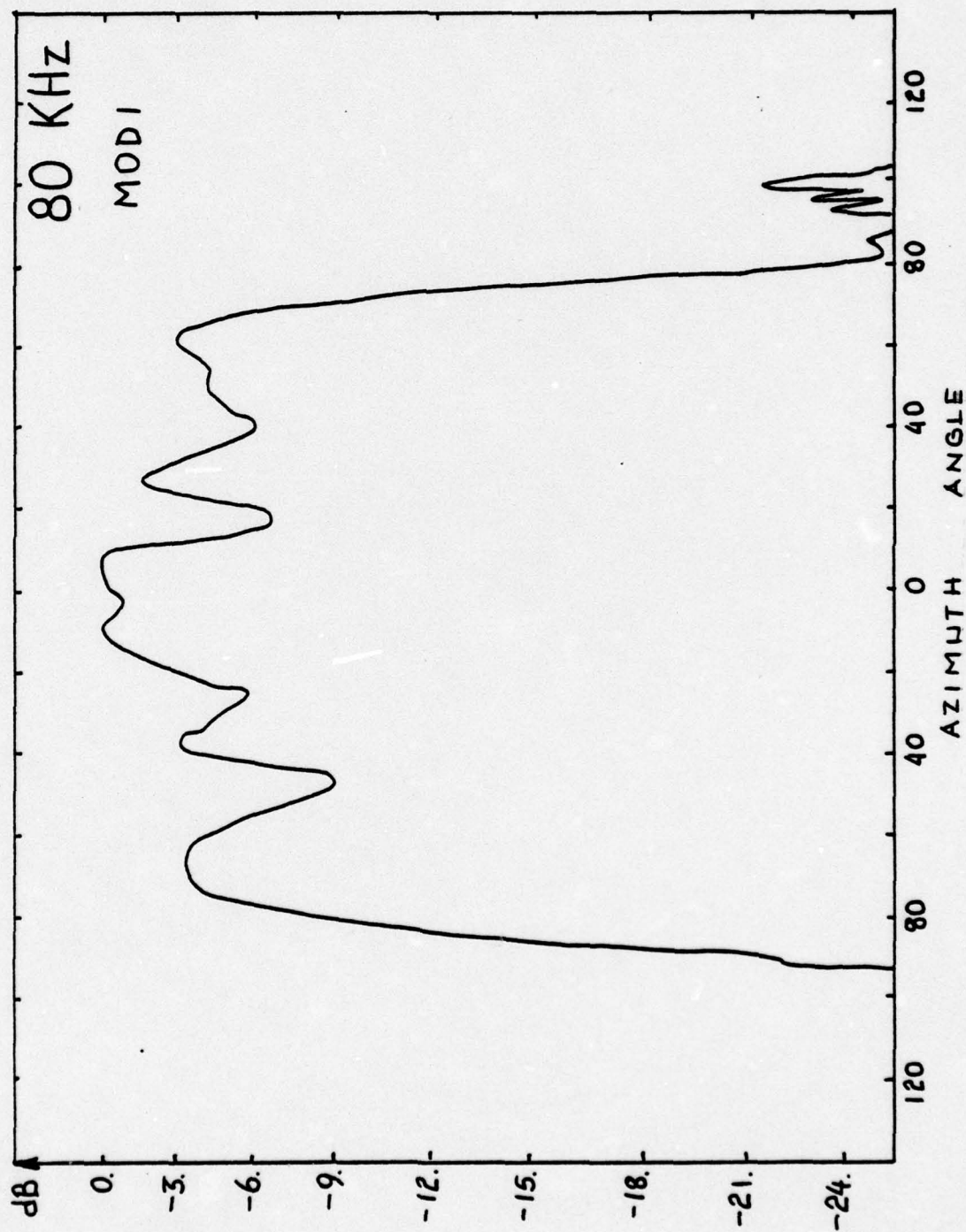


Figure 19 - RADIATION PATTERN

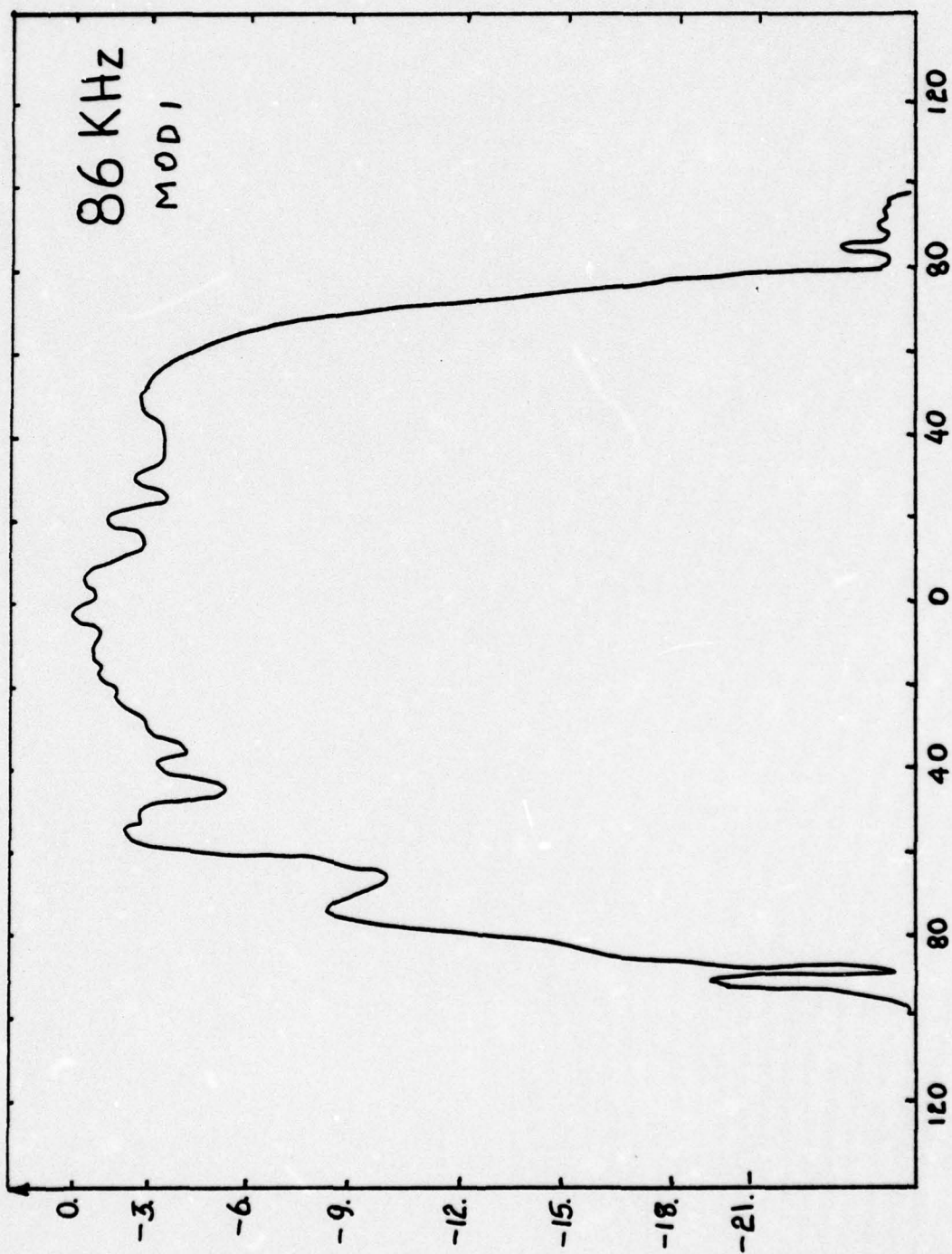
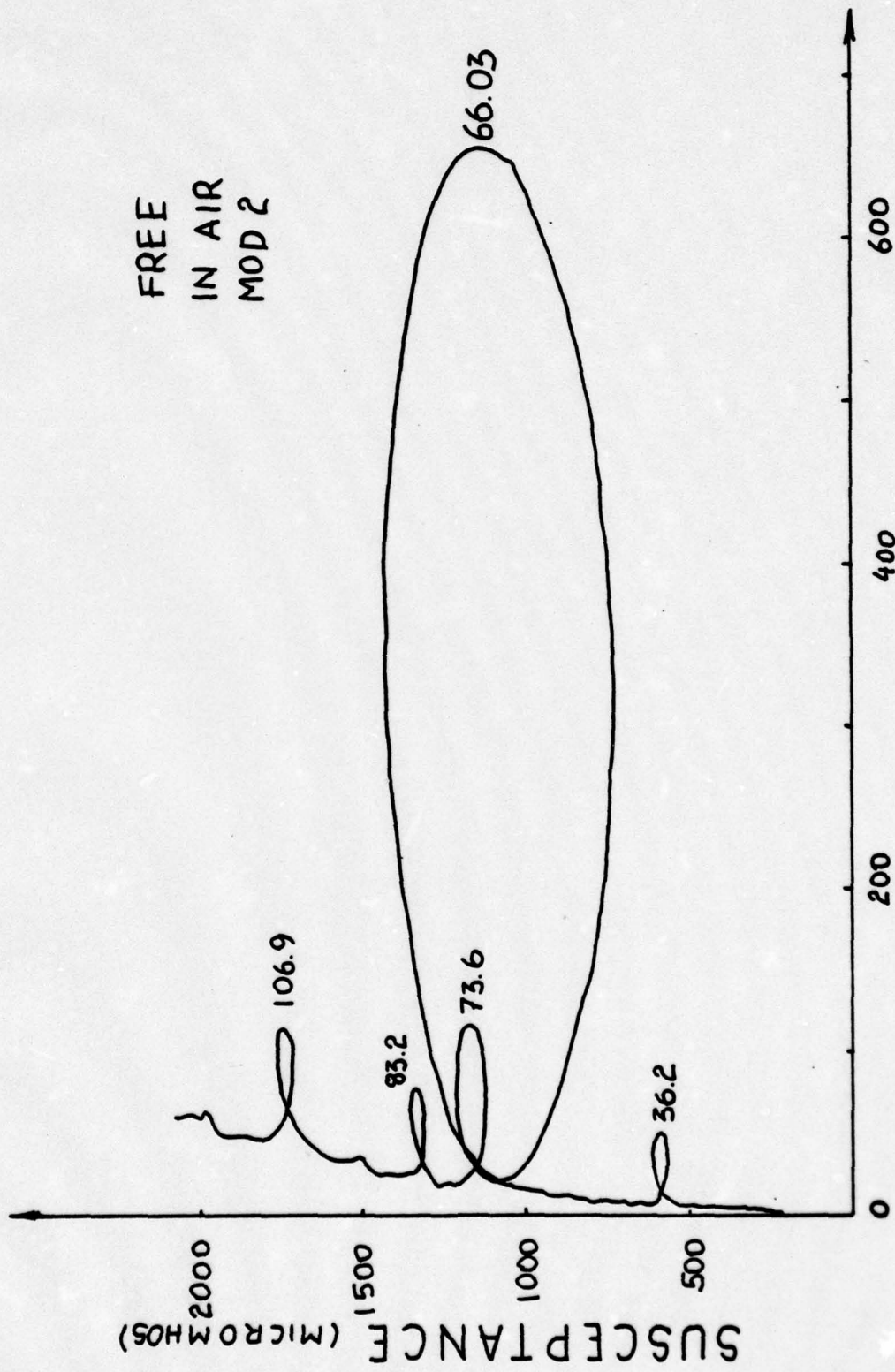
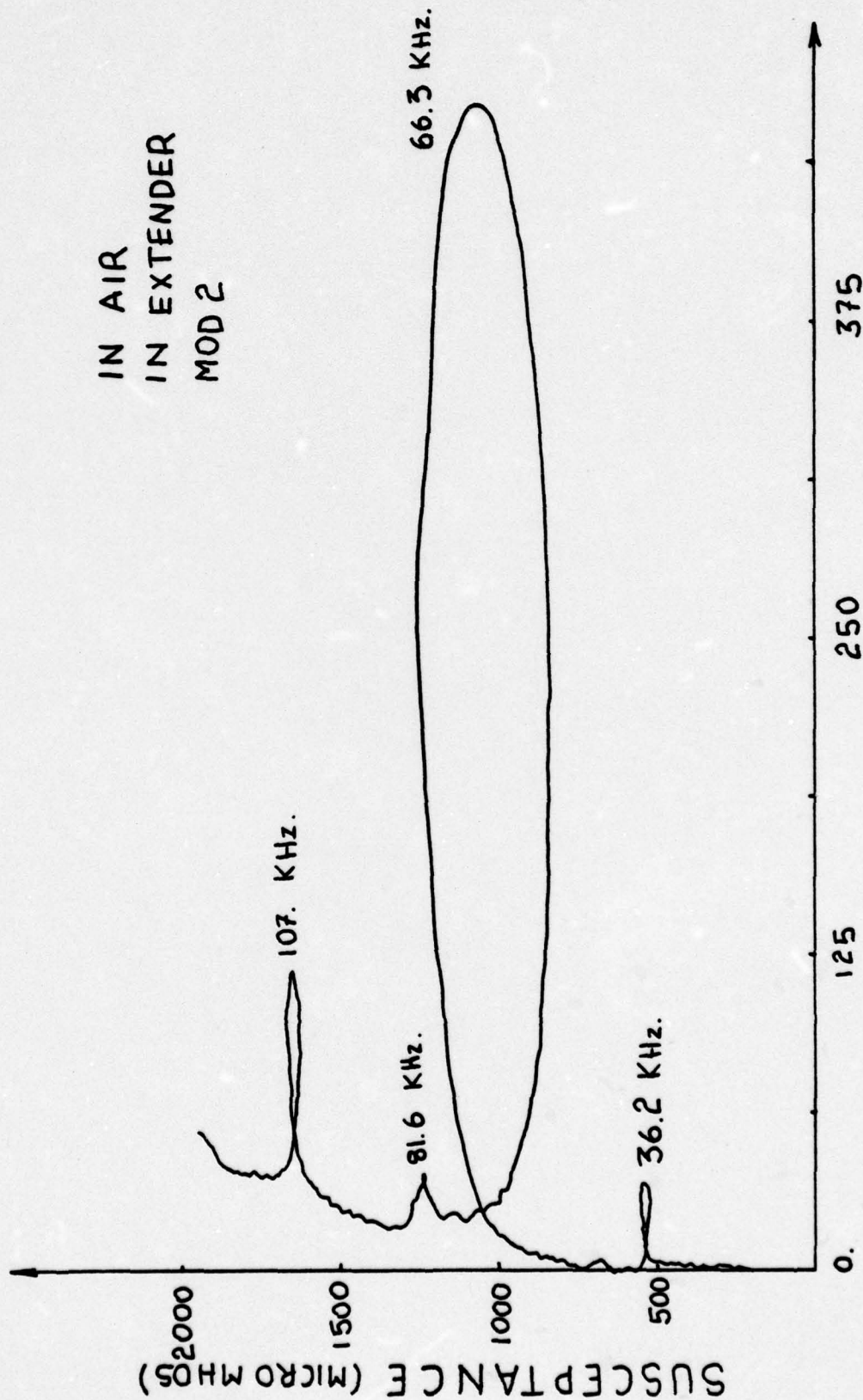


Figure 20 - RADIATION PATTERN



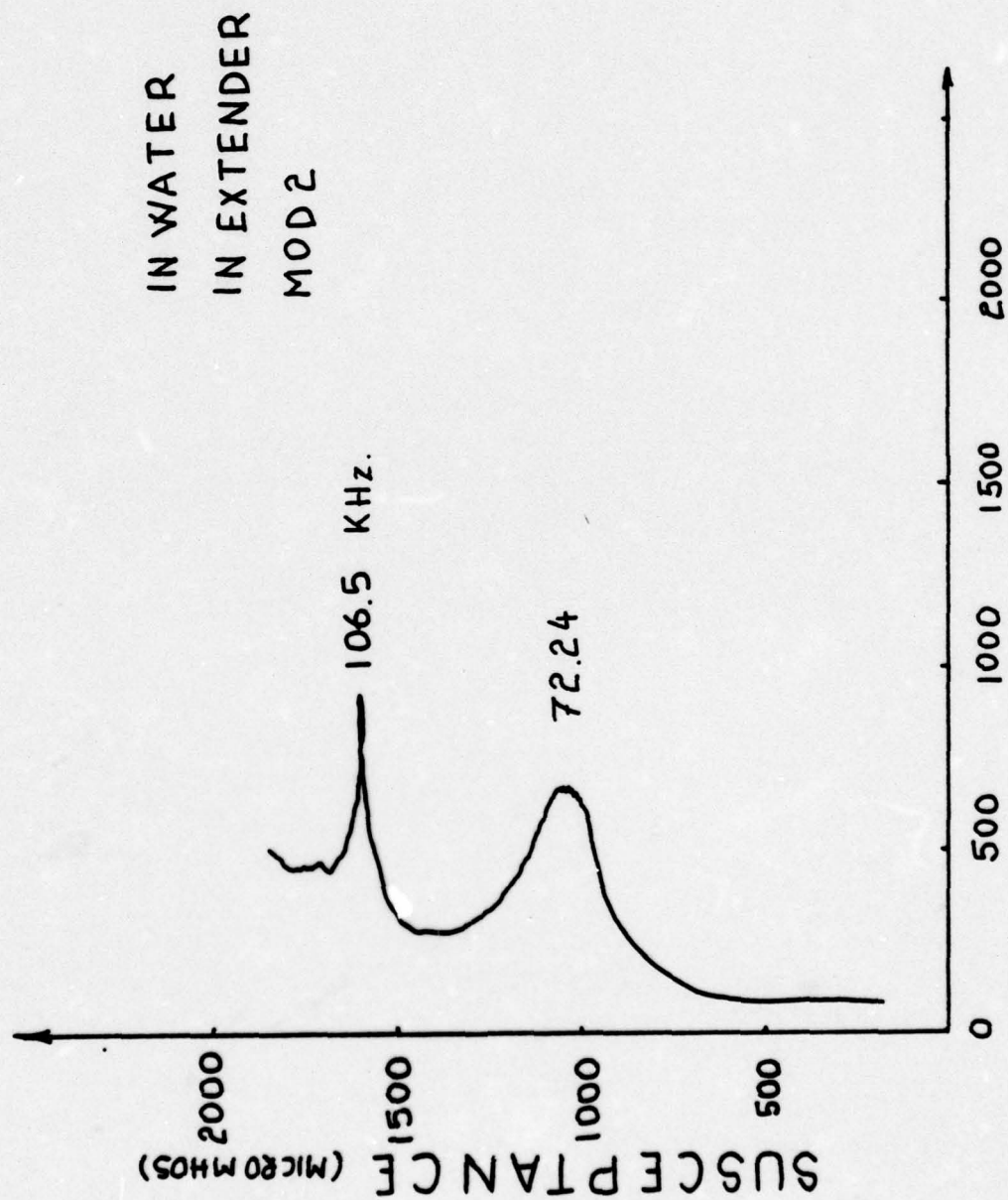
CONDUCTANCE (MICROMHOS)
Figure 21 - ADMITTANCE MEASUREMENT

IN AIR
IN EXTENDER
MOD 2



CONDUCTANCE (MICROMHOS)

Figure 22 - ADMITTANCE MEASUREMENT



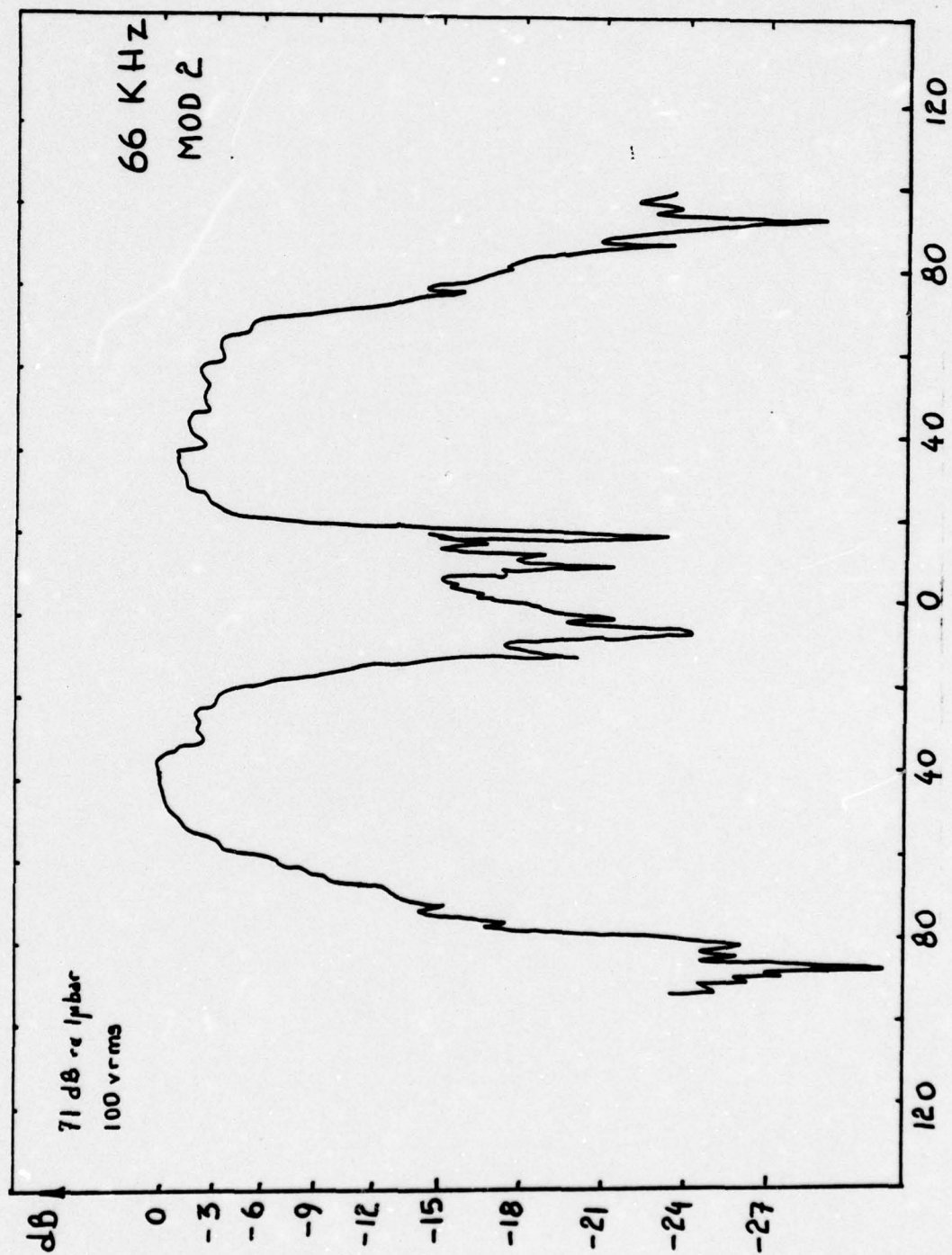


Figure 24 - RADIATION PATTERN

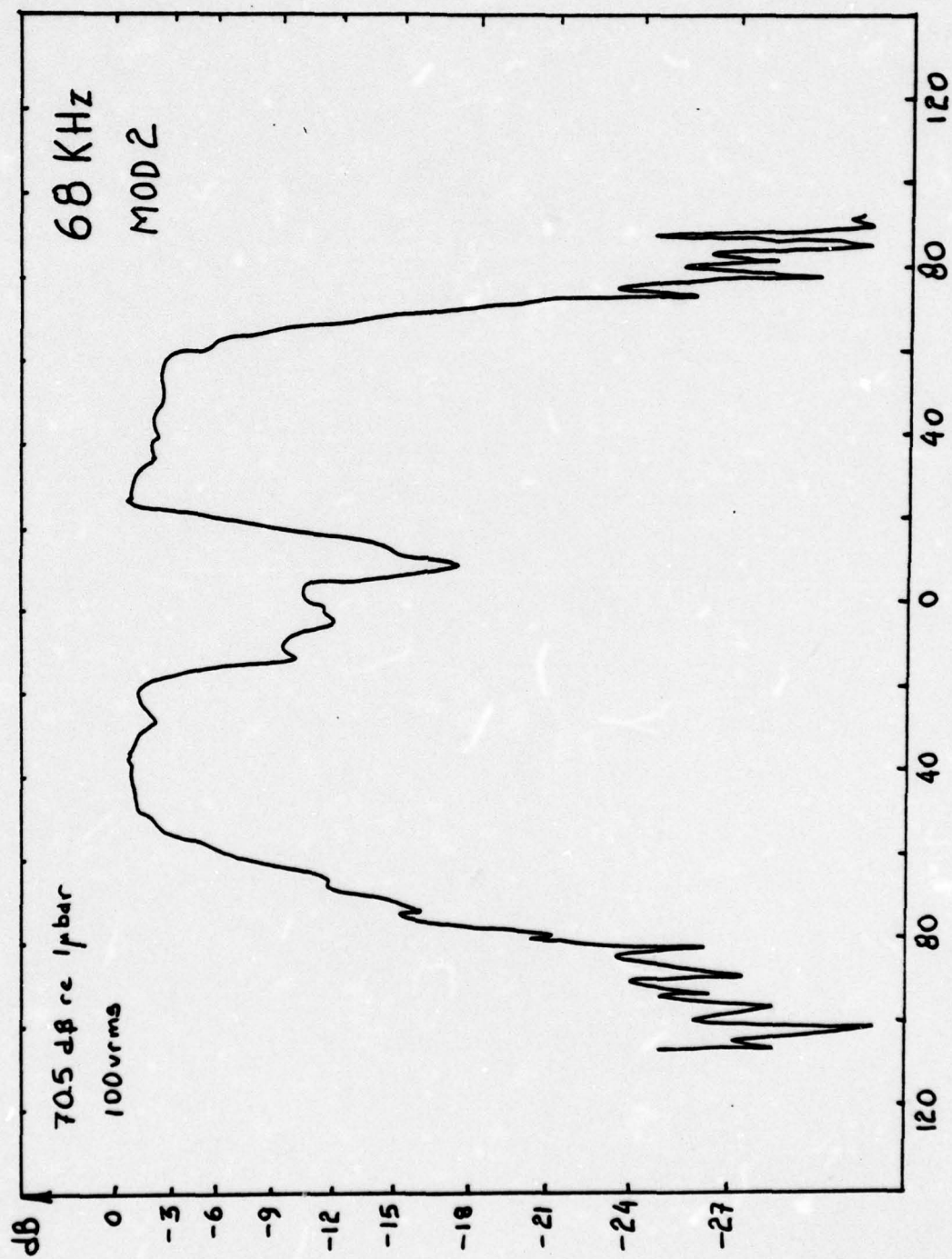


Figure 25 - RADIATION PATTERN

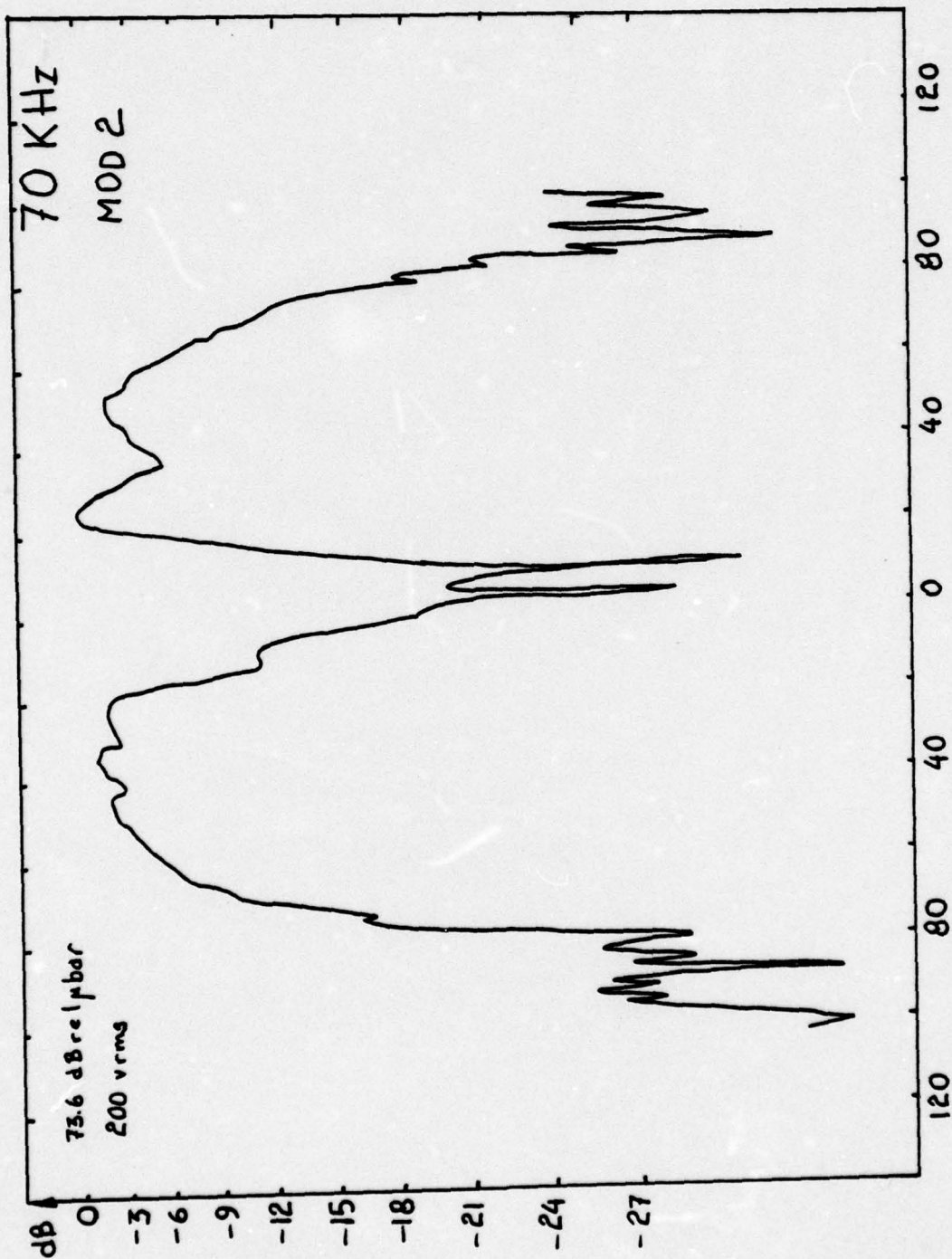


Figure 26 - RADIATION PATTERN

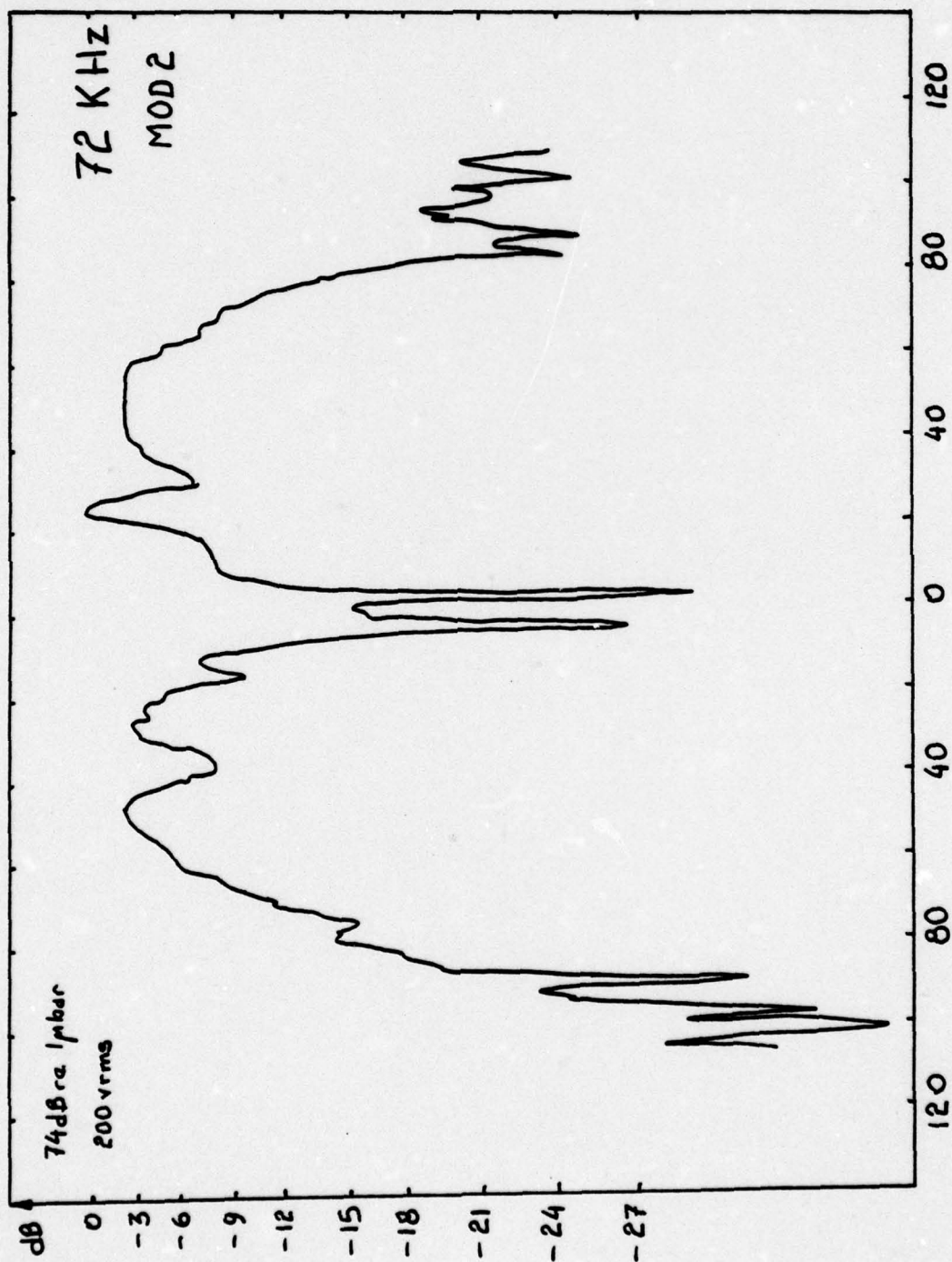


Figure 27 - RADIATION PATTERN

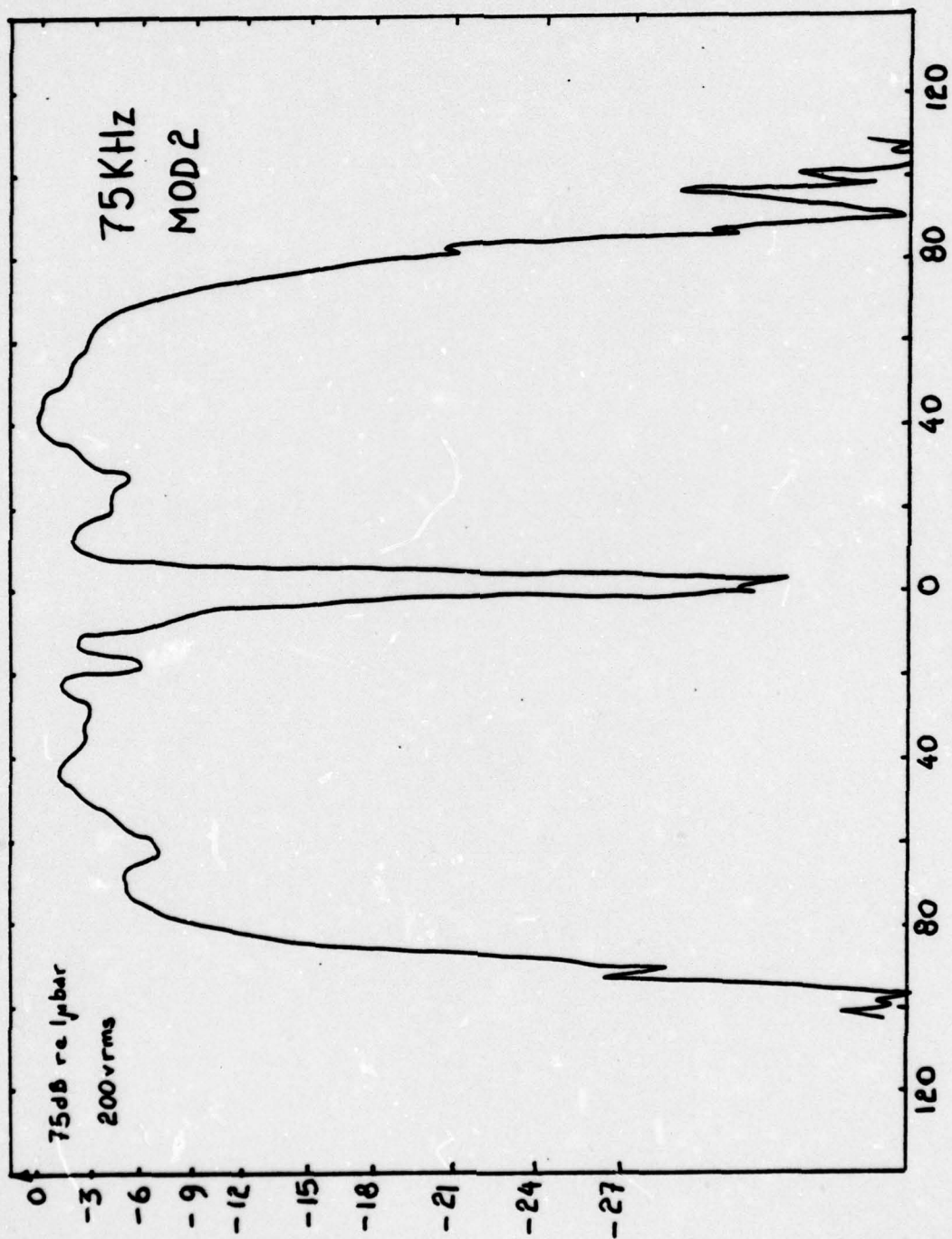


Figure 28, - RADIATION PATTERN

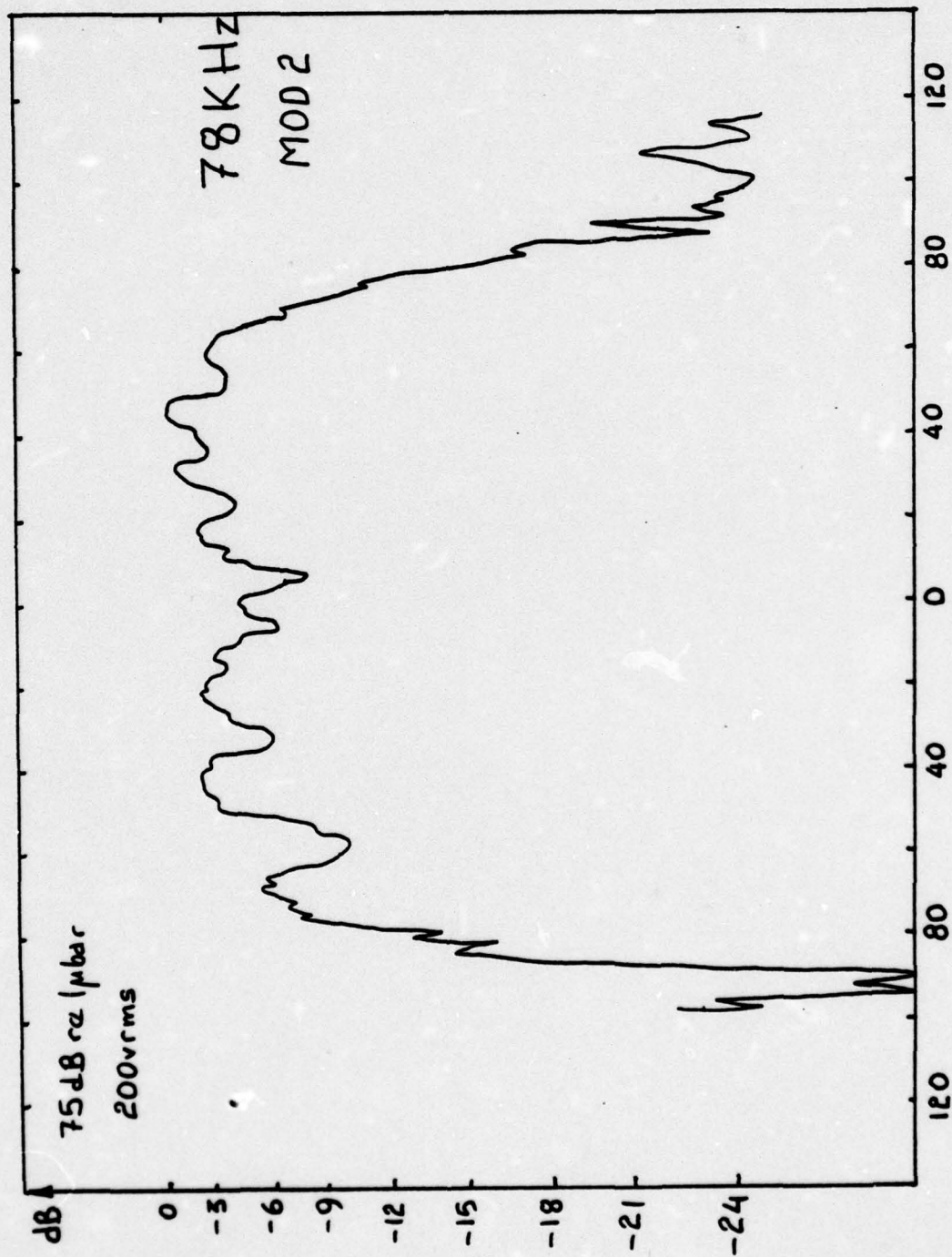


Figure 29 - RADIATION PATTERN

72.24 KHz
MOD 1

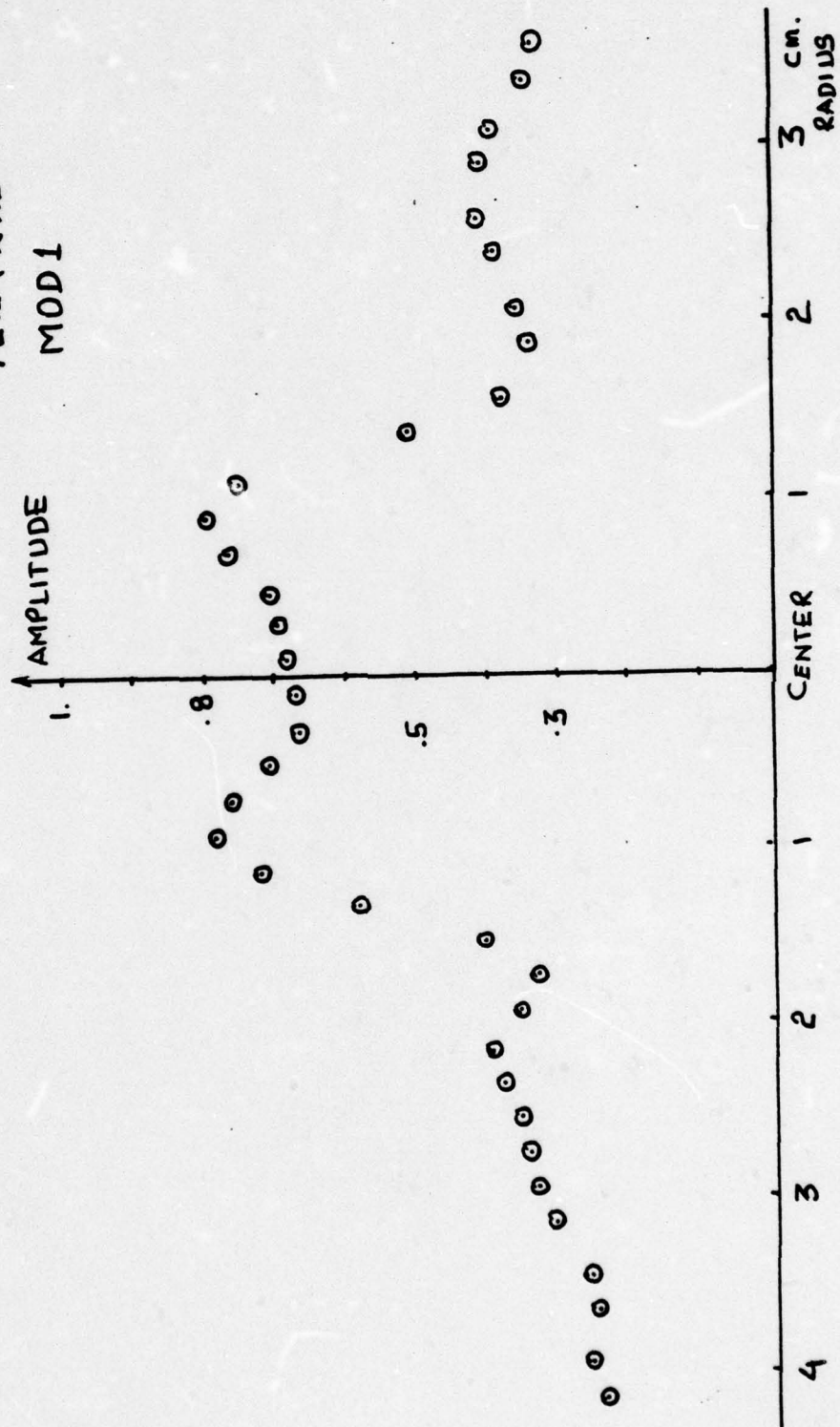


Figure 30 - NEAR FIELD PRESSURE AMPLITUDES

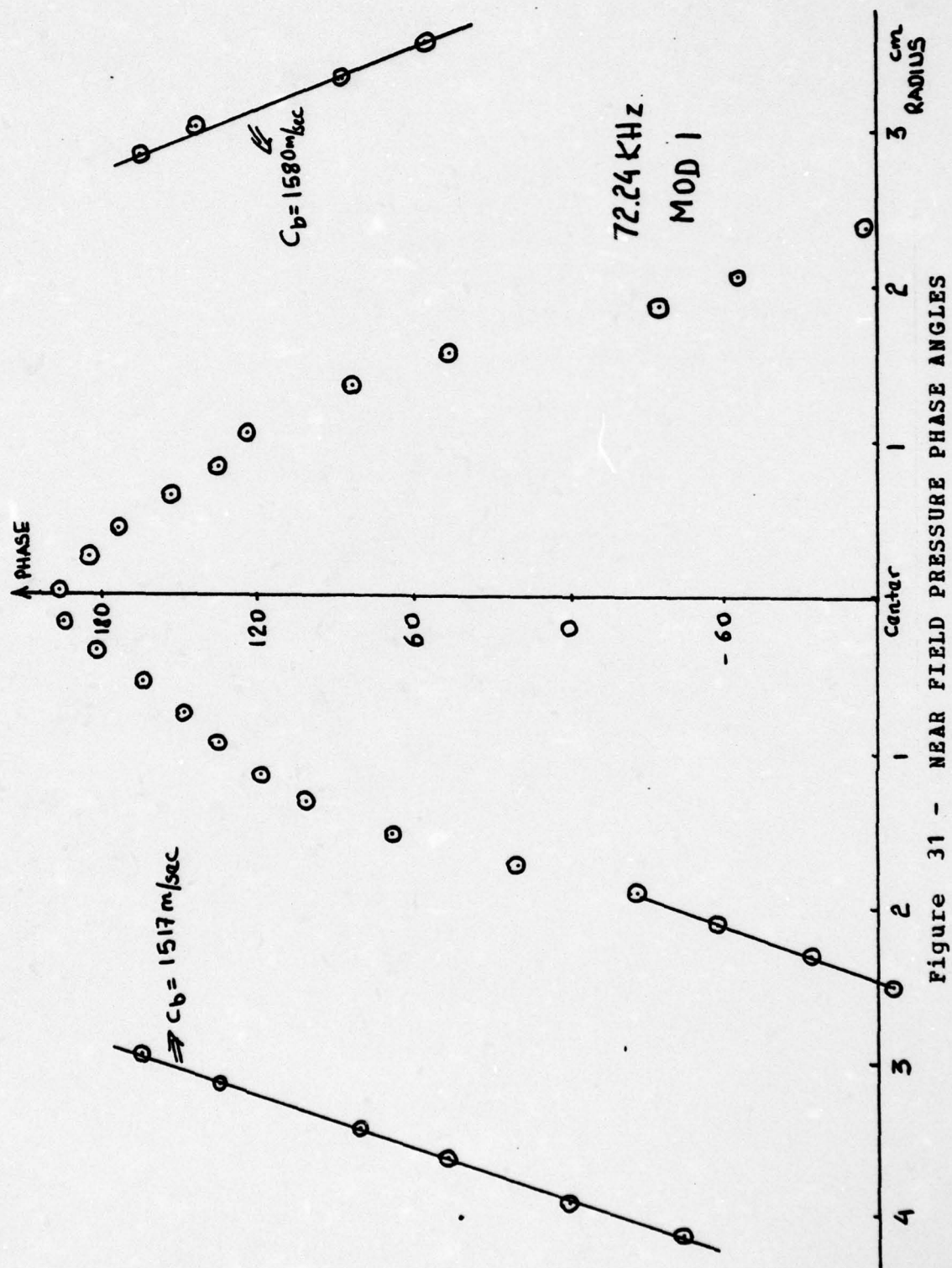


Figure 31 - NEAR FIELD PRESSURE PHASE ANGLES

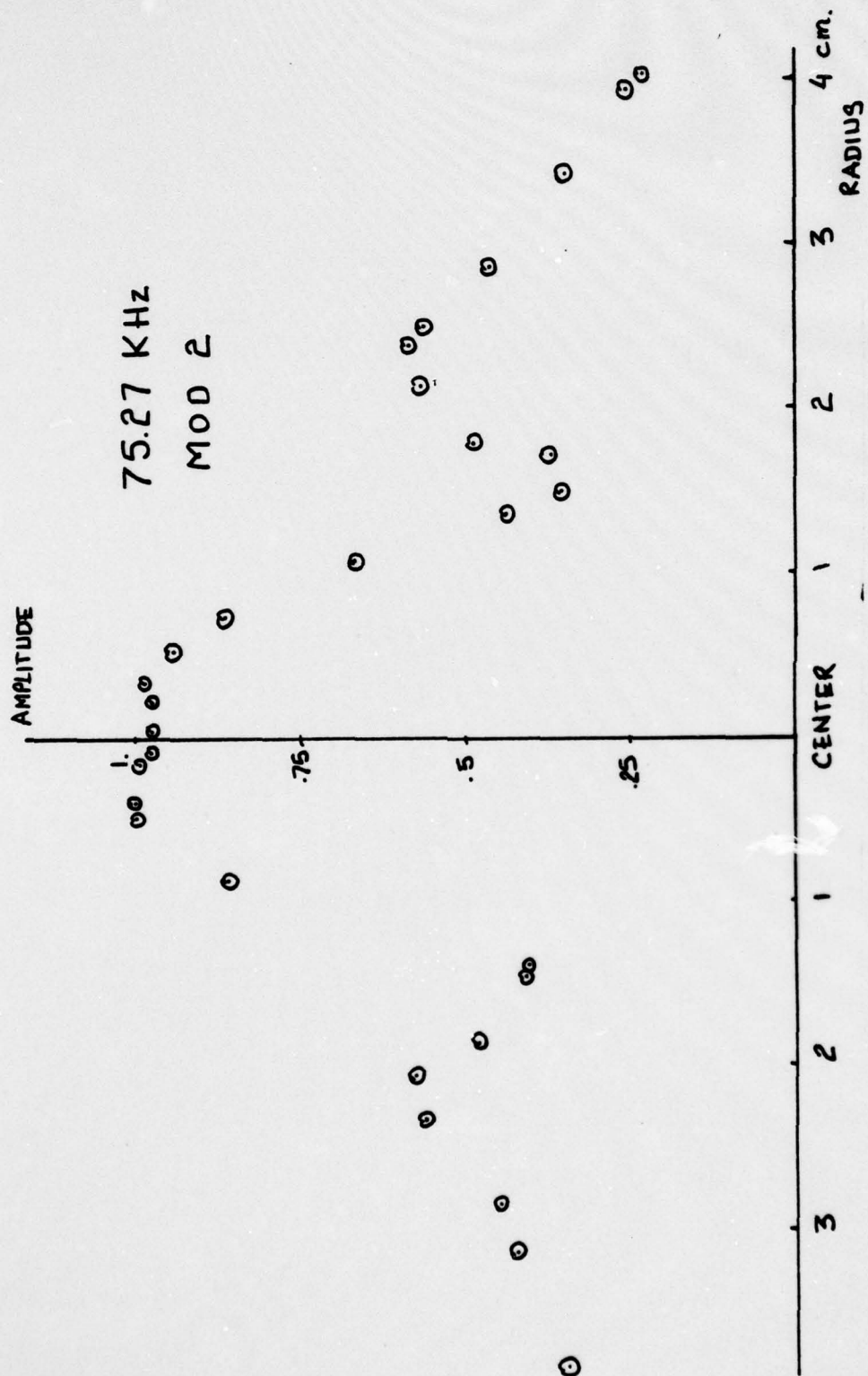


Figure 32 - NEAR FIELD PRESSURE AMPLITUDES

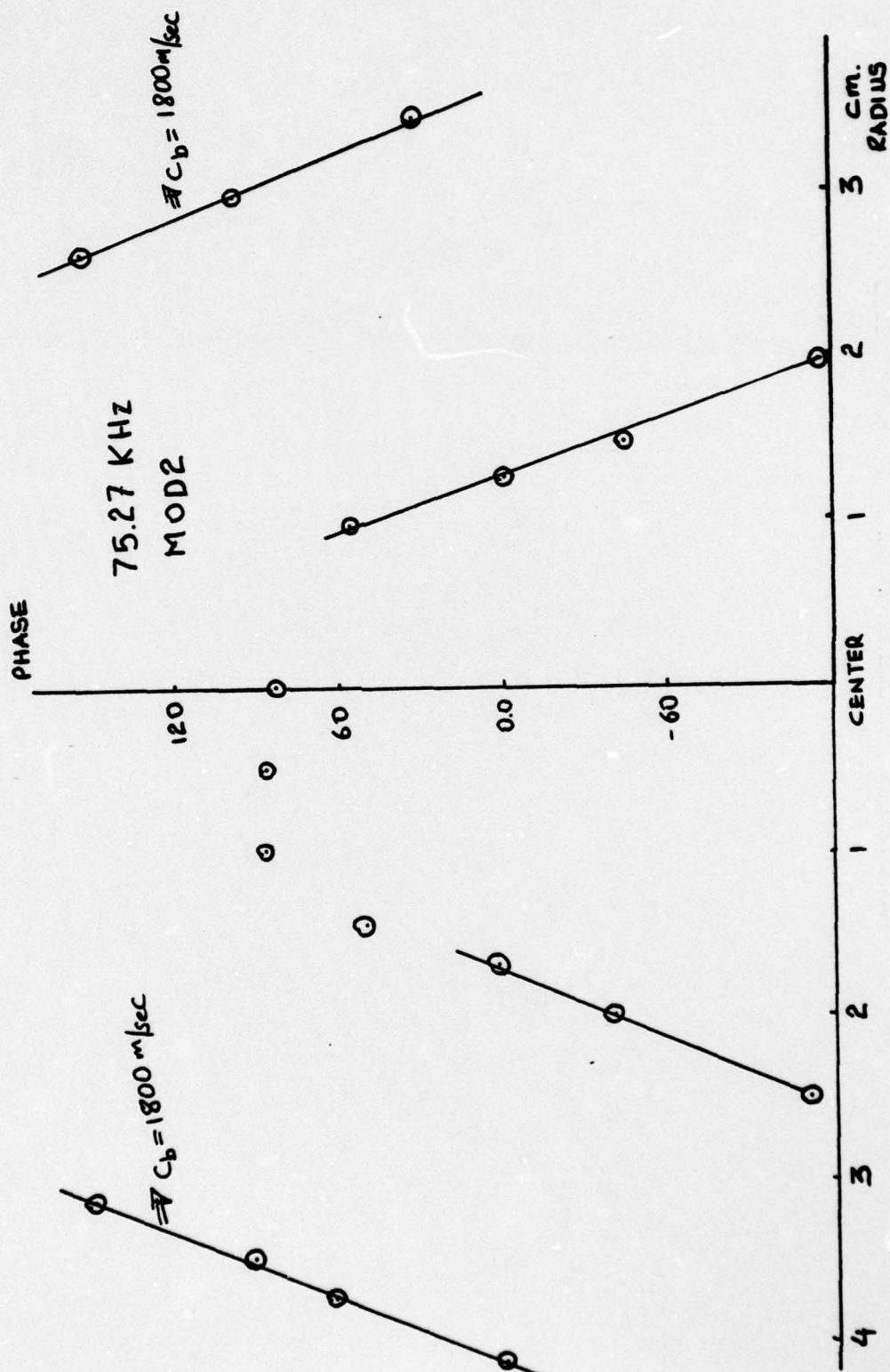


Figure 33 - NEAR FIELD PRESSURE PHASE ANGLES

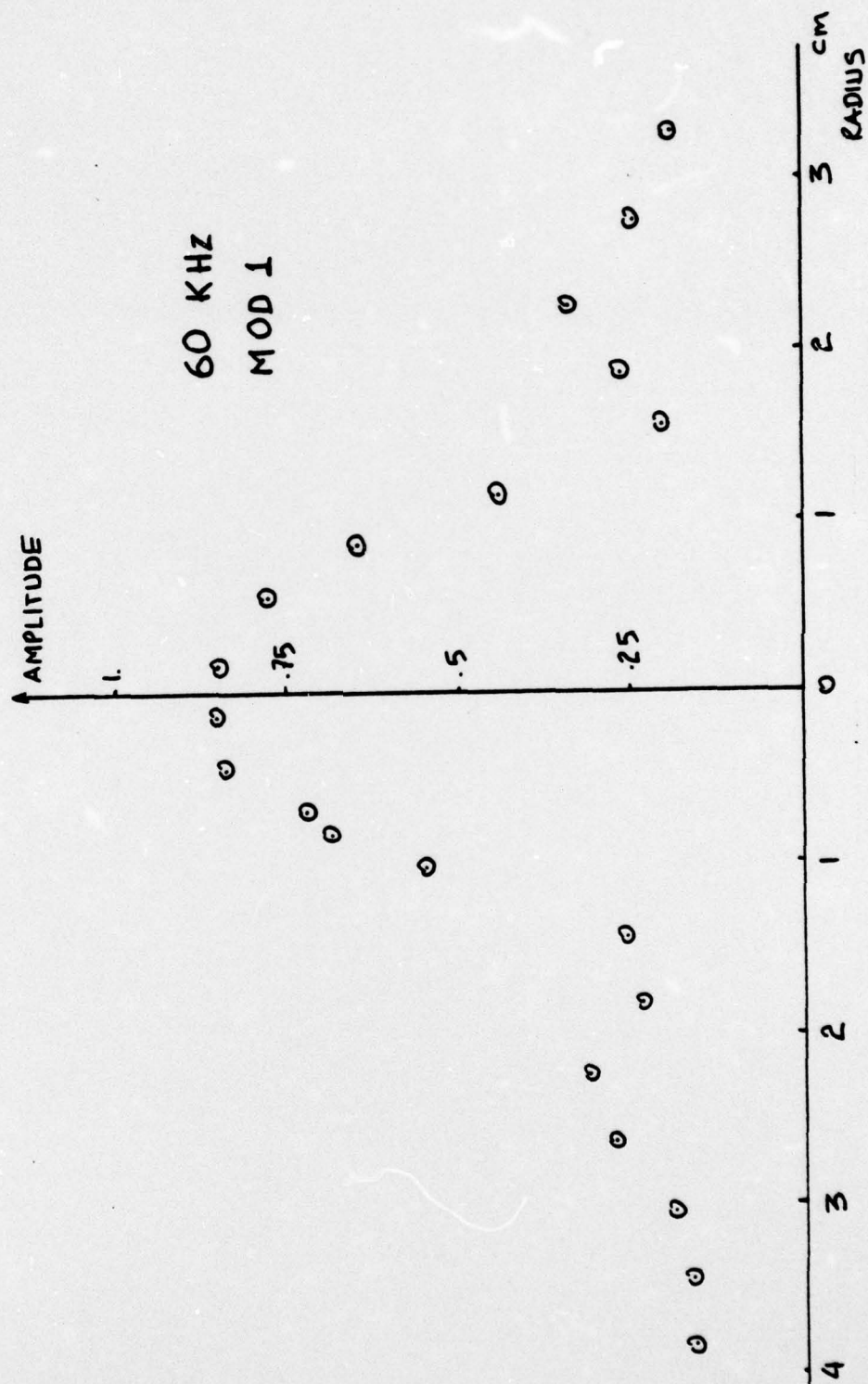


Figure 34 - NEAR FIELD PRESSURE AMPLITUDES

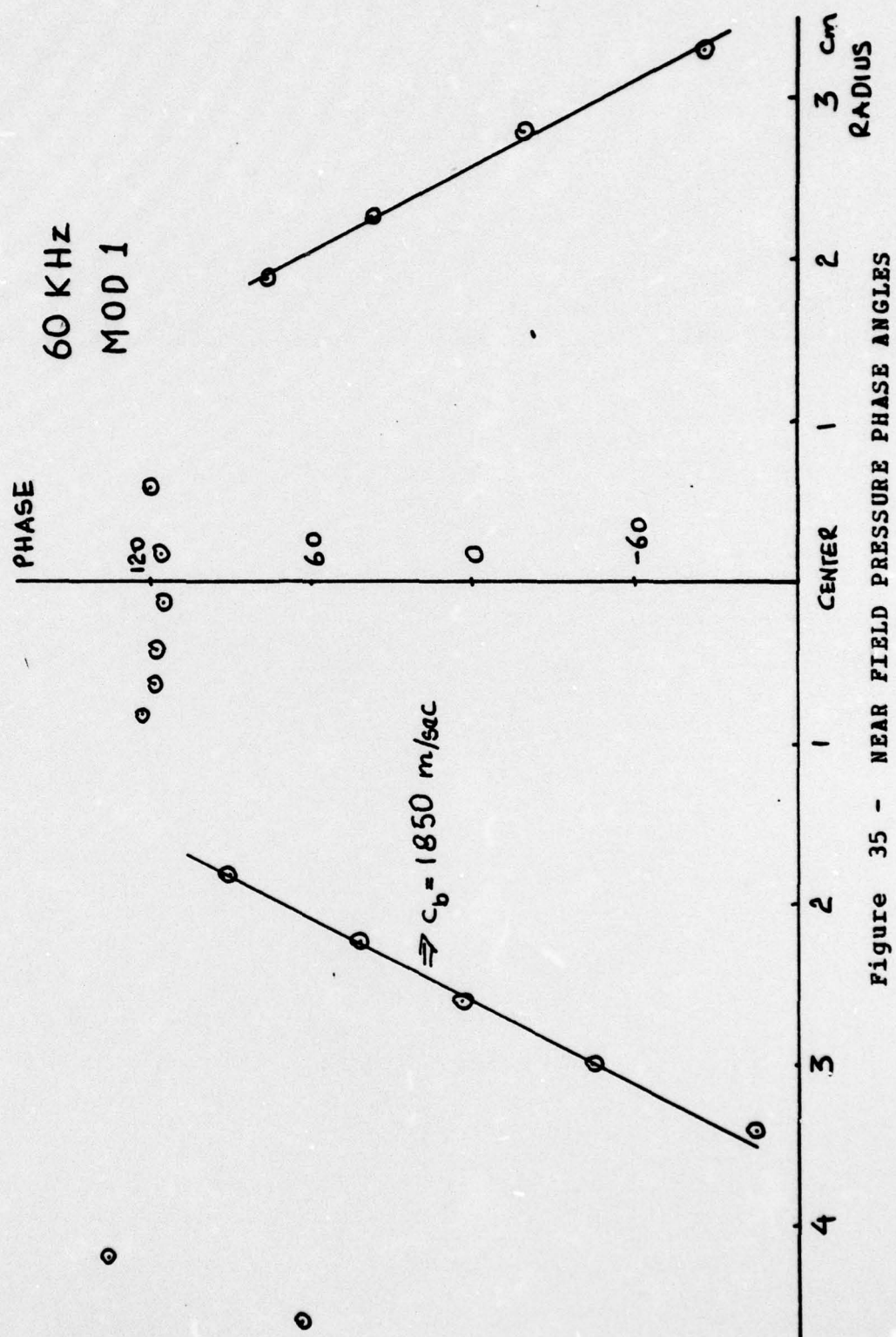


Figure 35 - NEAR FIELD PRESSURE PHASE ANGLES

IV. SUMMARY OF AND DISCUSSION OF RESULTS AND SOME CONCLUSIONS

There are some discrepancies between predicted normal mode frequencies and those actually measured which are difficult to account for quantitatively. They are most likely due to violations of the thin plate assumption and perhaps due to coupling between the modes of the plate with those of the longitudinal driver vibrator.

From the admittance curves obtained when in water, the only resonance frequencies appear to be those of the driving element.

This forces the conclusion that the radiation resistance completely damps the normal mode flexural resonances in the plate. The radiation which does occur then must be due to flexural waves propagating radially outward from the driver element located at the center of the plate.

This conclusion is also supported somewhat by the results of the near field measurements. In Figs 30, 32, 34, it is seen that the pressure amplitude is essentially constant over a diameter about equal to that of the driver element. Thus, the central part of the plate is behaving as a uniformly driven piston. The change in phase with radius along the plate beyond this center region corresponds to a wave speed which is higher than that in water. The phase speed of the flexural waves should increase with frequency and with plate thickness according to theory. In the three sets of data taken, the increase in phase speed with thickness was observed. The effect with frequency was

inconsistent and could not be explained.

For the reason just stated the theoretical radiation patterns calculated based on the assumption of a propagating flexural wave from a point source should not be realized, because the source is not a point.

The radiation patterns observed for the two models, shown in Figs 13-20 and Figs 24-29 can be summarized in the accompanying table (Table I). The values of the angles to the outermost -6 dB points are tabulated at various frequencies. Any dip in response along the axial direction is also noted.

There is a consistent assymetry in the patterns which disappeared when a pattern was taken with a plane baffle. This is due to the location of the radiator nearer to one end of the cylindrical extender section used as baffle for these measurements.

The angular widths to the -6 dB points are large, varying between about 120 to 148 degrees at frequencies which cover a band width more than 6 kHz on either side of resonance. These compare favorably to the 135 degrees width specified by the Naval Torpedo Station (Ref. NAVORD 2814382 Fig 2, Modified 2-28-73, Flush 3-D Transducer Output Specifications).

The change in source level with frequency is not more than 4 dB in the band width between 60-80 kHz.

The desired dip in source level at angles near the axis is not found at all frequencies. In fact, near resonance, there appears to be a small peak near the axis. It is not possible to account for these quantitatively. The reduction found in axial source levels is probably not broad enough to

be significantly useful in reducing overall power requirements.

The maximum source level observed near resonance was about 75 dB ref. 1 microbar at 1 meter. This was for a 200 volt rms drive voltage applied, which was the maximum undistorted value available with the equipment used in these tests. From the data on the electrical admittance, the conductance at resonance is 700 micromhos. Thus at this drive voltage, the input power is about 28 watts during the pulse.

According to private communications from NTS, the desired 93 dB source level is achieved with about 400 watts input power during the pulse. It is seen that this transducer, if driven with 400 watts, and if it were linear in response, would have a maximum source level of about 87 dB, about 6 dB less than that desired.

TABLE I

| FIG No. | f kHz | OUTER -6dB ANGLES | | WIDTH | INNER -6dB ANGLES | | WIDTH | MAXIMUM SOURCE LEVEL | REMARKS |
|-------------------|----------|----------------------|------------|-------------|----------------------|-------|-------|-------------------------|--|
| | | LEFT | RIGHT | | LEFT | RIGHT | | | |
| M O D I | | | | | | | | | |
| 13 | 56 | 80 | 57 | 137 | 26 | 10 | 36 | | -15 dB |
| 14 | 60 | 56 | 68 | 124 | 15 | 15 | 30 | 70dB 140vrms | -10 dB |
| 15 | 66 | 80 | 68 | 148 | | | | | One sharp min. not on the axis -5dB |
| 16 | 70 | 80 | 60 | 140 | | | | | Two sharp dips each side of axis |
| 17 | 75 | 25 -12dB [92] | 32 [72] | 57 [154] | | | | 72dB 140vrms | Peak on axis |
| 18 | 77 | 77 | 70 | 147 | | | | | Peak along axis |
| 19 | 80 | 78 | 69 | 147 | | | | | Several dips small peak on axis |
| 20 | 86 | 60 | 66 | 126 | | | | | Essentially Flat |
| M O D I I | | | | | | | | | |
| 24 | 66 | 59 | 70 | 129 | 18 | 22 | 40 | 71dB 100vrms | Dip ~ 22 dB |
| 25 | 68 | 56 | 63 | 119 | 15 | 21 | 36 | 70.5dB 100vrms | Several dips, mostly -12dB |
| 26 | 70 | 61 | 65 | 126 | 15 | 19 | 34 | 73.6dB 200vrms | 2 sharp -30dB dips |
| 27 | 72 | 60 | 66 | 126 | 15 | 20 | 35 | 74 dB 200vrms | 2 sharp -30dB dips |
| 28 | 75 | 72 | 68 | 140 | 9 | 9 | 18 | 75dB 200vrms | One deep min. -30dB |
| 29 | 78 | 68 | 68 | 136 | - | - | - | 75dB 200vrms | 2 or 3 dips below -6dB |
| S P E C I F I C D | | | | | | | | | |
| | 75 | 67 | 67 | 135 | | | | | Minimum 93dB re 1μbar source level is required |

V. RECOMMENDATIONS

Because of the promising results mentioned above , further study is recommended.

The electromechanical efficiency can probably be improved somewhat if piezoelectric ceramic elements more suitable for this application were chosen. For example, one should use ceramic elements for the vibrator which have parallel field coupling and appropriate composition. The 33 coupling instead of the 31 coupling used here should increase the electromechanical coupling coefficient and give a larger operating band width. The ceramic composition should be one designed for high power use (The Glennite HS-21 used here is more appropriate for hydrophone use).

Some problems which must also be addressed if this approach is to be of practical use:

The obtaining of a curved face to fit the curvature of the torpedo. This could be achieved by a rubber window which has same ρ_c as water which is molded to the flat disk.

The radiation face of the transducer could be made larger with a possible resulting increase the source level.

Further experimental tests on the effect of plate thickness with rubber window in place are recommended. An empirical approach is necessary to determine optimum plate thickness to get the desired radiation pattern.

APPENDIX A

COMPUTER PROGRAM FOR NORMAL MODE SOLUTION

```

100 DIMENSION A(20),U(21),PTZ(20),DARG(20),X(30),Y(30),UDIF(20)
110 FJ(20)
120 R=RADIUS(M.)
130 BE=2.007
140 U(21)=0.
150 PI=3.14159
160 PK=2.*PI*75000./1500.
170 FORMAT(4X,E12.5,10X,E12.5)
180 C=PI*BE
190 CALL BESJ(C,0,DJ,.1,IER)
200 DO 17 M=1,20
210 ABOB=1.
220 XM=M
230 Z=C*XM/20.
240 H=(Z/2.)*2
250 DO 15 I=1,6
260 ABT=1.
270 DO 16 K=1,I
280 FACT=ABT*K
290 ABT=FACT
300 CONTINUE
310 SQF=ABT**2
320 AB=H**I/SQF+ABOB
330 ABOB=AB
340 CONTINUE
350 FJ(M)=ABOB
360 CONTINUE
370 EJ=FJ(20)
380 DO 1 I=1,20
390 YI=1
400 A(I)=R/20.*YI
410 PTZ(I)=A(I)**2
420 B=C*YI/20.
430 CALL BESJ(B,0,8J,.1,IER)
440 U(I)=BJ-DJ*FJ(I)/EJ
450 WRITE(6,100)A(I),U(I)
460 CONTINUE
470 TOT=0.
480 DO 2 I=1,20
490 K=K+1
500 UDIF(I)=U(I)-U(K)
510 AXP=PTZ(I)*UDIF(I)+TOT
520 TOT=AXP
530 CONTINUE
540 PTZA=ABS(TOT)/2.
550 WRITE(6,300) PTZA
560 FORMAT(//,2X,'AXIS PRESSURE',2X,E12.5)
570 FORMAT(//,3X,'ANGLE',10X,'PRESSURE',14X,'DECIBEL')

```

```

WRITE(6,500)
DO 4 I=1,30
J=3*I
X(I)=J
TH=X(I)/57.29578
ATOT=0.
DO 5 K=1,20
ARGO=PK*A(K)*SIN(TH)
CALL BESJ(ARGO,1,BJ,1.1ER)
DARG(K)=BJ*PTZ(K)/ARGO
5 CONTINUE
DO 6 M=1,20
PTI=DARG(M)*UDIF(M)+ATOT
ATOT=PTI
6 CONTINUE
PDB=20.*ALOG10(ABS(PTI/PTZA))
WRITE(6,400)J,PTI,PDB
400 FORMAT(4X,I3,8X,E12.5,8X,F10.3)
Y(I)=PDB
4 CONTINUE
CALL PLOTP(X,Y,30,0)
STOP
END

```


APPENDIX B

COMPUTER PROGRAM FOR PROGRESSIVE WAVE SOLUTION

```

100 DIMENSION UR(20),UI(20),PTZ(20),DARG(20),X(30),Y(30),Z(30),
110 URDIF(20),UIDIF(20),A(20)
120 FORMAT(4X,E12.5,10X,E12.5)
130 FORMAT(4X,PTZM=,E12.5,F1X=,F5.2)
140 FORMAT(4X,13,10X,E12.5,10X,F5.2)
150 FORMAT(//,3X,ANGLE,10X,PTOTM,14X,FTOT)
160 H=HALF THICKNESS (M.)
170 R=RADIUS (M.)
180 UR(21)=0.
190 UI(21)=0.
200 PI=3.14159
210 PK=2.*PI*75000./1500.
220 WM=12.257/H**.5
230 WK=WM*R
240 DO 1 I=1,20
250 RK=WK*I/20.
260 CALL BESJ(RK,0,BJ,1,IER)
270 CALL BESY(RK,0,BY,IEB)
280 A(I)=R/20.*I
290 PTZ(I)=A(I)**2
300 WRITE(6,100)BY,BJ
310 UR(I)=BY
320 UI(I)=BJ
330 CONTINUE
340 1 CALC AXIS PRESSURE
350 TOTR=0.
360 TOTI=0.
370 DO 2 I=1,20
380 K=I+1
390 URDIF(I)=UR(I)-UR(K)
400 UIDIF(I)=UI(I)-UI(K)
410 AXPR=PTZ(I)*URDIF(I)+TOTR
420 TOTR=AXPR
430 TOTI=AXPI
440 WRITE(6,200)TOTR,TOTI
450 CONTINUE
460 2 PTZAM=ABS((TOTR*TOTR+TOTI*TOTI)**.5)/2.
470 FIAX=ATAN(TOTI/TOTR)
480 WRITE(6,300)PTZAM,FIAX
490 WRITE(6,500)
500 CALC PRESSURE FROM AXIS
510 DO 4 I=1,30
520 J=3*I
530 X(I)=J
540 TH=X(I)/57.29578
550 ATOT=0.

```



```

BTOT=0.
DO 5 K=1,20
  ARGQ=PK*A(K)*SIN(TH)
  CALL BESJ(ARGQ,1,BJ,1,IER)
  DARG(K)=BJ*PTZ(K)/ARGQ
5 CONTINUE
DO 6 M=1,20
  PTIR=DARG(M)*URDIF(M)+ATOT
  PTII=DARG(M)*UIDIF(M)+BTOT
  ATOT=PTIR
  BTOT=PTII
6 CONTINUE
  TOT=ATOT+BTOT*BTOT)**.5
  PTOTM=(ATAN(BTOT/ATOT)
  FTOT=ATAN(BTOT/ATOT)
  PDB=20.*ALOG10(ABS(PTOTM/PTZAM))
  FREL=FTOT-FIAX
  Y(I)=PDB
  Z(I)=FREL
  WRITE(6,400)J,PTOTM,FTOT
4 CONTINUE
  CALL PLOTP(X,Y,30,0)
  CALL PLOTP(X,Z,30,0)
  STOP
  END

```

LIST OF REFERENCES

1. Morse and Ingard, Theoretical Acoustics, p. 213 to 217, Mc Graw Hill, 1968.
2. Malecki, Physical Foundations of Technical Acoustics, p. 505 to 523, Pergamon Press, 1969.
3. Kinsler and Frey, Fundamentals of Acoustics, p. 502, John Wiley and Sons, 1962.
4. Shaw, A.H.P., Radiation Pattern of a Two-Element, Concentric Ring Transducer Using Phase and Amplitude Shading, M.Sc. Thesis, Naval Postgraduate School, 1975

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